

November 2020 Kittitas County Conservation District The Ranch on Swauk Creek Diversion Improvement and Restoration Project



# Design Report

Prepared for Kittitas County Conservation District



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#### **Prepared for**

Kittitas County Conservation District 2211 W. Dolarway Road, Suite 4 Ellensburg, Washington 98926 **Prepared by** 

Anchor QEA, LLC 1201 3rd Avenue, Suite 2600 Seattle, Washington 98101

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### **ABBREVIATIONS**

cfs cubic foot per second
CMP corrugated metal pipe

CPE corrugated high-density polyethylene

ESA Endangered Species Act

fps feet per second

KCCD Kittitas County Conservation District
NAVD88 North American Vertical Datum of 1988

NMFS National Marine Fisheries Service

project The Ranch on Swauk Creek Diversion Improvement and Restoration Project

RCO Washington Recreation and Conservation Office

RM River Mile

SRFB Salmon Recovery Funding Board USACE U.S. Army Corps of Engineers

USGS U.S. Geological Survey

WDFW Washington Department of Fish and Wildlife

WRIA Water Resource Inventory Area

WSEL water surface elevation

YTAHP Yakima Tributary Access and Habitat Program

#### 1 Introduction

This Design Report was prepared for The Ranch on Swauk Creek Diversion Improvement and Restoration Project (project). The project is being implemented by Kittitas County Conservation District (KCCD), with the support of the Washington Department of Fish and Wildlife (WDFW) and with grant funding from the Washington Recreation and Conservation Office (RCO) through the Salmon Recovery Funding Board (SRFB).

KCCD proposes to restore fish passage and conserve instream flow in a reach of Swauk Creek by consolidating two gravity irrigation diversions that serve The Ranch on Swauk Creek to a single point of diversion. The project will also pipe portions of the irrigation conveyance ditch on the ranch to reduce evaporation and infiltration losses, and it will include planting cottonwood copses in strategic locations to provide shade and future woody debris for the stream and floodplain. This report outlines project objectives and constraints, summarizes how the project objectives have been addressed through the key elements incorporated into the design of the project, and includes analyses completed as a basis for the design of the project.

## 1.1 Project Background

The Yakima River basin has been modified by a complex array of reservoirs, diversion dams, canals, and drains used to divert and convey water for over 100 years. Humans have modified the timing and quantity of river and streamflows in the Yakima River and several of its tributaries. Tributaries to the Yakima River, especially those that do not have large dams and are not subject to storage reservoir operations, offer excellent opportunities to improve salmonid rearing habitat. KCCD has been working with the Yakima Tributary Access and Habitat Program (YTAHP) technical group, local agencies, and irrigators to improve fish passage on tributaries to the Yakima River in Kittitas County.

The proposed project is located on Swauk Creek, northwest of Ellensburg in Kittitas County. Swauk Creek is a tributary to the Yakima River. The Swauk Creek watershed drains an area of about 100 square miles before entering the Yakima River at River Mile (RM) 170. Swauk Creek is an important and productive spawning and rearing stream for Endangered Species Act (ESA)-listed steelhead, spring Chinook salmon, coho salmon, ESA-listed bull trout, and other species. Like other tributaries to the upper Yakima River, flow in Swauk Creek is largely derived from snow during the winter months and snowmelt in the spring. The upper Yakima River limiting factors analysis (Haring 2001) identified that low flows (or sometimes no flows) in lower Swauk Creek severely limit steelhead production and may preclude coho salmon spawning because flows are typically lowest in the fall.

Two irrigation diversions draw water from Swauk Creek at RM 7.71 and RM 7.92 to supply The Ranch on Swauk Creek, just upstream of where the creek crosses under U.S. Highway 97. The irrigation diversions are not screened in accordance with current National Marine Fisheries Service (NMFS) and

WDFW screening guidelines, resulting in mortality of fish when they are trapped in the irrigation systems. The diversions also represent partial barriers to fish migration.

The proposed project will consolidate the irrigation diversions into a single point of diversion with a fish screen that meets current WDFW fish-screening guidelines. The project will also correct fish passage barriers at the two existing points of diversion, convert a portion of an earthen delivery ditch to a buried pipeline to reduce evaporation and infiltration, and restore riparian areas by planting cottonwood copses in key locations to provide shade and future woody debris for the stream.

#### 1.2 Prior Work

The current irrigation headgate and screen system was replaced in 2010 to reduce entrainment of fish in the irrigation ditch system. A short, steep rock ramp was installed at that time to raise the water elevation in the creek to allow for diversion at the upper headgate. This rock ramp shifted during high flows and no longer holds Swauk Creek to a sufficient elevation to maintain irrigation diversions throughout the irrigation season. A vertical flat plate screen with a propeller-driven mechanical brush was also installed in 2010, but the hydraulic conditions at the screen have not provided the appropriate velocities needed to move fish and debris past the screen and through the bypass back to the creek. In addition, the outlet of the fish bypass pipeline frequently becomes buried in sediment and is difficult to maintain.

## 1.3 Project Purpose

The overall purpose of the project is to improve fish passage and conserve instream flows in Swauk Creek by consolidating two gravity irrigation diversions on Swauk Creek to a single point of diversion, piping an irrigation conveyance channel to reduce evaporation and infiltration, and planting cottonwood copses in strategic locations to provide shade and future woody debris for the stream and floodplain. The design and implementation of key project elements are intended to achieve the following specific project objectives:

- Eliminate irrigation-related mortality of steelhead, coho, and Chinook salmon at Swauk Creek RM 7.71 and significantly reduce the irrigation-related mortality of steelhead, coho, and Chinook salmon at Swauk Creek RM 7.92.
- 2. Restore year-round fish passage for all life stages of salmonids at Swauk Creek RM 7.71 and RM 7.92.
- 3. Improve summer rearing conditions for juvenile steelhead, coho, and Chinook salmon in Swauk Creek by increasing irrigation efficiency, resulting in up to 0.25 cubic foot per second (cfs) of conserved water (approximately 8% of the water right) available for instream flow benefits.

4. Increase canopy cover, provide shade, and produce a source of future large woody debris for Swauk Creek and its floodplain by planting up to approximately 3.5 acres with cottonwood copses.

## 1.4 Report Organization

This report includes the following sections:

- Section 2, Project Location and Existing Conditions: Describes existing conditions at the proposed project site and summarizes the design criteria and requirements for the project.
- Section 3, Proposed Improvements: Describes the proposed improvements at the project site.
- **Section 4, Design Criteria:** Lists the design criteria used in the development of project improvements.
- Section 5, Design Analyses: Summarizes the analyses completed to evaluate project
  alternatives, select a preferred project alternative, and develop the design of the project.
- Section 6, Summary of Proposed Improvements: Summarizes the key facilities included in the design of the project.
- Section 7, Opinion of Probable Construction Cost: Includes the opinions of probable project
  costs developed as part of the design and identifies cost considerations that have been
  evaluated and refined as part of the final design phase of the project.
- **Section 8, Summary and Recommendations:** Provides an overall summary and recommendations for design development and implementation.

## 2 Project Location and Existing Conditions

This section includes a brief description of the project site and its existing conditions.

#### 2.1 Location

The proposed project is located on Swauk Creek (Water Resource Inventory Area [WRIA] 39), northwest of Ellensburg, Washington, in Kittitas County (Figure 2-1). The two irrigation diversions are located in the northwest quarter of Section 27, Township 20N, Range 17E, just upstream of where Swauk Creek crosses U.S. Highway 97 near the intersection of U.S. Highway 97 and Washington State Route 970.

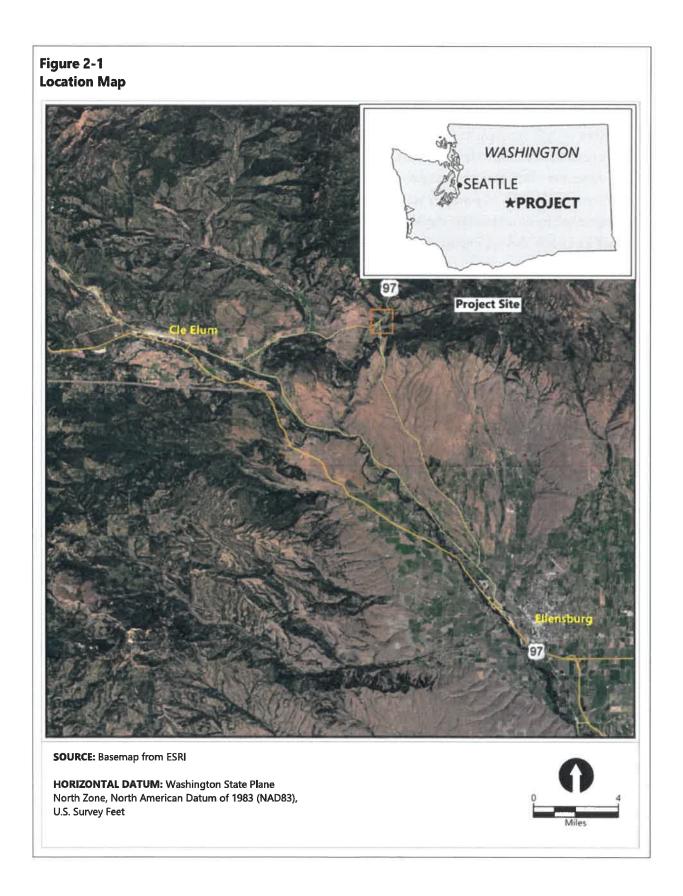
## 2.2 Existing Conditions

Existing conditions were observed during a site visit on April 29, 2020. Notes and photographs taken during the site visit are included as Appendix A. Key characteristics of Swauk Creek and the existing irrigation facilities at the site are summarized as follows.

#### 2.2.1 Swauk Creek

Swauk Creek originates in the Wenatchee Mountains (a northwest-southeast trending spur of the Cascade Mountains) near Diamond Head peak (elevation 5,915 feet), just south of Blewett Pass. It flows for approximately 23 miles to its confluence with the Yakima River near RM 170. The Swauk Creek watershed is approximately 100 square miles. Swauk Creek drains approximately 83 square miles upstream of the project site. The upstream diversion is at an elevation of 2,191 feet (North American Vertical Datum of 1988 [NAVD88]). The basin is fed by multiple small tributaries. Like other tributaries to the upper Yakima River, the hydrology of Swauk Creek is defined by high spring and early summer flows driven by snowmelt, with low late summer and early fall flows. Although the drainage area of Swauk Creek is fairly large, precipitation in the Swauk Creek watershed is low, with the majority coming in the form of snow during the winter months. Late-summer low flow in lower Swauk Creek limits steelhead production and may preclude coho salmon spawning.

Aerial photography shows that most of the basin is forest canopy with no development. Previous logging is evident by the location of forest roads and drag marks. The creek channel in the upper portions of the drainage basin is steep, at an average grade of greater than 20%. However, the channel becomes flatter at approximately 2% grade through the last 10 miles of the basin upstream from the project site. The mean basin slope is approximately 33.6%.



A substantial number of commercial and private interests conducted gold prospecting throughout the upper Swauk Creek watershed in the late 1800s and early 1900s. The resulting impacts of mining activities are still apparent today. The relatively high degree of fine sediment within the system is a likely result of the long history of suction dredging. In addition, many of the coarse materials (boulders and cobbles) were dredged out of the creek and placed in mounds adjacent to the creek. In the mid-1950s, U.S. Highway 97 was constructed, and Swauk Creek was channelized and straightened to accommodate the highway. The cumulative effect of these actions has reduced large wood and pools that are important components of stream function and aquatic habitat.

#### 2.2.1.1 Out-of-Stream Water Needs and Water Rights

The Ranch at Swauk Creek relies on Swauk Creek to provide stock water and irrigation water for up to 118.2 acres of pasture for raising of horses and livestock. The Ranch at Swauk Creek currently has water rights that allow for diversion of surface water from Swauk Creek of up to 2.0 cfs at RM 7.92 and up to 1.5 cfs at RM 7.71.

#### 2.2.1.2 Fish Species Present

The primary fish species of concern in Swauk Creek listed under the ESA is mid-Columbia summer steelhead trout. Swauk Creek also provides habitat for ESA-listed spring Chinook salmon, ESA-listed bull trout, coho salmon, Pacific lamprey, cutthroat trout, and rainbow trout. NMFS identified the upper Yakima local steelhead population as being at high risk (NMFS 2011). Radio telemetry data from 2002 to 2014 indicate that 13% of upper Yakima steelhead spawn in Swauk Creek (USBR 2006; Temple et al. 2015). Table 2-1 provides a summary of the key fish species that may be present at the site.

Table 2-1
Key Fish Species Potentially Present at Project Site

Species	Endangered Species Act Coverage	Adult Migratory Season	Juvenile Migratory Season
Middle Columbia Summer Steelhead	Yes, Threatened	April to May	March to May
Coho Salmon	No	October to November	April to May
Spring Chinook Salmon	No	September	October to November
Columbia River Bull Trout	Yes, Threatened	October to November	Year-round
Pacific Lamprey	No	April to July	November or March to April

Upper Yakima steelhead hold in the mainstem river during the winter months and migrate to tributaries for spawning in the spring, possibly related to water temperature (Yakima Subbasin Fish

and Wildlife Planning Board 2004). Steelhead would thus be migrating through the creek during or just following the spring snowmelt runoff.

### 2.2.2 Irrigation Diversion at RM 7.92

The irrigation diversion at RM 7.92 consists of the following key components:

- Headgate Structure: Flow from Swauk Creek to the irrigation system is controlled by a 4-foot-wide slide gate mounted on a reinforced-concrete inlet structure on the right bank (looking downstream) of the creek. The existing headgate and inlet structure appear to be in good condition and operate as designed.
- **Fish Screen**: The headgate controls flow through a short segment of unlined ditch to the existing fish screen. The fish screen is a vertical flat plate screen mounted in a fabricated metal structure that was originally provided by WDFW. The screen is self-cleaning with a mechanical brush that is driven by a propeller that rotates in the irrigation water as it discharges through the structure downstream of the screen. The screen appears to consistently keep fish from being entrained in the irrigation ditch but frequently backwaters. The hydraulic conditions at the screen do not maintain consistent sweeping velocities to move fish and debris past the screen and through the bypass back to the creek. During the irrigation season, the existing screen requires very frequent cleaning (as often as every 2 hours).
- **Fish Bypass**: An 8-inch fish bypass pipeline conveys excess water, fish, and debris back to the creek. The bypass outlet at the creek frequently becomes buried in sediment and it appears, at times, that water backs up in the bypass and flows toward the screen.
- Roughened Channel: A previous project constructed in 2010 created a small roughened channel
  and rock weir structure immediately downstream from the intake to back the water up into the
  intake. Streambed boulders were placed in the channel to create the weir. However, it appears
  that some streambed boulders have shifted or settled and are not able to maintain adequate
  hydraulic conditions to keep the appropriate depth or flow of water needed in the diversion
  during the late summer.

To operate the current diversion system and maintain diversions during the late summer, the property owner currently installs an aluminum pole across the stream channel with a plastic tarp attached to it and anchored to the streambed to back up the water. These materials placed in the channel create a complete fish passage barrier while in place.

#### 2.2.3 Diversion at RM 7.71

The diversion at RM 7.71 consists of the following key components:

 Headgate Structure: Flow from Swauk Creek to the irrigation system is controlled through a 16inch canal gate mounted on a reinforced-concrete inlet structure on the left bank of the creek.
 The existing headgate and inlet structure appear to operate as designed.

- Diversion Pipeline: The headgate controls flow to a 16-inch-diameter steel pipeline that
  conveys water to the irrigation system. A combination of buried pipeline and open ditch conveys
  water from the point of diversion to the fish screen.
- **Fish Screen:** This diversion includes a vertical flat plate screen mounted in a fabricated metal structure that was originally provided by WDFW, similar to the fish screen at the upper diversion. However, the screen is far off-channel and downstream of the diversion, approximately 500 feet from the point of diversion, between the headgate structure and Burke Road. The screen is self-cleaning with a mechanical brush that is driven by a propeller that rotates in the irrigation water as it discharges through the structure. Because the fish screen is far downstream of the diversion on the ditch system, fish become entrained in the diversion system and cannot easily be returned to the creek. In addition, the existing fish screen appears to overtop multiple times a year when diverted flows exceed the capacity of the fish screen. A fish bypass pipeline returns bypass flows and fish to Swauk Creek at a discharge point near the U.S. Highway 97 bridge. The bypass pipe does not meet current fish passage guidelines and, during low flow conditions, drops water more than 3 feet into the rocky stream channel at the outlet.

The diversion facilities, diversion pipeline and ditch, fish screen, and bypass are not located on property owned by The Ranch at Swauk Creek. These facilities are also much less accessible than the diversion facilities at RM 7.92.

The gradient of the stream channel at this location is very steep and does not provide adequate depth or flow conditions during the late summer to maintain irrigation diversions. In addition, the diversion pipe inlet is high relative to the channel, so it is difficult to divert water, even when there is some depth in the creek adjacent to the diversion. Currently the property owner installs cattle fencing with a plastic tarp attached to it and temporary pipe extending up the left bank of the creek to maintain diversions during the late summer low-flow period. The owner deploys these materials to the creek as early as July to maintain diversions through the irrigation season.

The temporary materials placed in the channel at this diversion create a fish passage barrier. In addition, there are two drops over boulders in the channel adjacent to the headgate that are at least 12 inches high and may preclude passage by some fish species and juvenile fish.

## 2.2.4 Irrigation Delivery System

The existing delivery system conveys water to points of use primarily through a system of open, unlined earthen ditches and culverts. Up to 2.0 cfs flows through the upstream diversion to an open ditch that extends more than 850 feet west, where it then crosses under U.S. Highway 97 through an existing 36-inch corrugated metal pipe (CMP) culvert. Approximately 360 feet west of U.S. Highway 97, the ditch branches. The main flow continues west to irrigate pasture on ranch property north and west of Swauk Creek. Excess water flows in the other branch of the ditch south

along Burke Road, where it crosses through a series of culverts under an access driveway and Ranch Road, before discharging to Swauk Creek.

Up to 1.5 cfs flows through the downstream diversion to a 16-inch steel pipeline. A combination of pipelines and open ditches conveys diverted water to the fish screen, which is approximately 500 feet downstream of the point of diversion. Water for irrigation passes through the fish screen and is conveyed via a combination of buried pipelines, culverts, and open ditches to a structure on the east side of Burke Road. The structure controls flow through a culvert under Burke Road and allows for overflow through a branching ditch and culvert to Swauk Creek. Water conveyed for irrigation continues under Burke Road through a 24-inch corrugated high-density polyethylene (CPE) culvert to an open ditch that conveys water to a pond located on ranch property south of Burke Road. Water from the pond is used to irrigate pasture south and east of Swauk Creek.

## 3 Proposed Improvements

The proposed improvement project is shown on the design drawings included as Appendix B. These drawings represent design of a preferred alternative that was selected after evaluation of other potential design alternatives considered and summarized in Section 5 of this report. The project will consolidate the two gravity irrigation diversions on Swauk Creek at RM 7.92 and RM 7.71 to a single point of diversion, at the location of the existing upstream point of diversion (RM 7.92). The diversion facilities at RM 7.92 will be upgraded to handle the combined flow and address existing deficiencies. Improvements will also be made to the roughened channel at that location. The fish screen and bypass pipeline will also be replaced. The diversion facilities at RM 7.71 will be removed and the left bank of the stream channel will be restored. Segments of open irrigation ditches will be piped to conserve water. Cottonwood copses will be planted to enhance the riparian area along the creek west of Burke Road. These improvements are summarized as follows.

#### 3.1 Diversion at RM 7.92

The diversion facilities at RM 7.92 will be upgraded to include a new rotating drum fish screen and fish bypass pipeline. Immediately downstream of the diversion, a roughened channel will be constructed to improve fish passage. The roughened channel design will include a low-flow channel approximately 80 feet long with a constructed slope of 2.5%. A gravel-cobble-boulder mix will be installed approximately 42 inches deep along the roughened channel section. Disturbed bank slopes and other areas will be revegetated by hydroseeding.

#### 3.2 Diversion at RM 7.71

The diversion facilities at RM 7.71 will be abandoned by removing the structures in the stream, removing the first 20 feet of diversion piping, and plugging the remaining pipe with non-shrink grout. Disturbed bank slopes and other areas will be graded to a 2:1 slope and revegetated by hydroseeding.

## 3.3 Irrigation Delivery System

Portions of the existing open, unlined ditch conveyance system will be replaced with buried delivery pipelines to conserve water. The pipelines will deliver water from the upgraded diversion at RM 7.92 to locations south of Burke Road. The first section of conveyance pipeline will follow the general alignment of the existing ditch on the north side of Swauk Creek for approximately 850 feet from the intake to U.S. Highway 97 where it will discharge water under the highway through the existing culvert. Water conveyed under U.S. Highway 97 in the culvert will flow into a pipeline on the other side of the highway which will terminate approximately 360 feet downstream in a manhole, where the flow will be split. Up to 2.0 cfs will be conveyed to the west through a short segment of pipe to an open ditch that delivers water for irrigation of pasture on ranch property north and west of Swauk

Creek. Up to 1.5 cfs will be conveyed to the south through a pipeline that will cross Swauk Creek and deliver water to an open ditch that conveys water to a pond on ranch property south and east of Swauk Creek.

## 3.4 Riparian Planting

Up to approximately 3.5 acres of cottonwood copses will be planted in gaps in the riparian growth along Swauk Creek west of Burke Road. The cottonwood copses will provide shade and a future source of large woody debris for Swauk Creek and its floodplain. This work will be done by a volunteer crew or under a separate contract than the construction contract used to complete the diversion and irrigation system improvements.

## 4 Design Criteria

#### 4.1 Design Flow Rates

Based on the analysis of available hydrologic data and WDFW fish passage design requirements, the following key flow rates and velocity criteria were identified for use in designing intake, piping, fish passage, and channel restoration improvements.

- Design flow rate for combined irrigation diversion = 3.5 cfs
- Design flow rate to pasture on north/west side of Swauk Creek = 2.0 cfs
- Design flow rate to pasture on south/east side of Swauk Creek = 1.5 cfs
- Low design flow for upstream adult fish passage = 4.6 cfs (80% overall exceedance flow)
- High design flow for upstream adult fish passage = 264 cfs (10% exceedance flow during the month of April for steelhead migratory season)
- 2-year flow = 356 cfs (channel-forming flow to inform design of channel restoration)
- 100-year flow = 1,180 cfs (peak flow to ensure channel stability, prevent upstream flooding)
- Maximum average channel velocity during high design flow (264 cfs) = 4.0 feet per second (fps)

## 4.2 Intake and Fish Screening Facilities

Fish screening facilities are required to meet the most current requirements for screening of diversions from WDFW and NMFS *Anadromous Salmonid Passage Facility Design Guidelines* (NMFS 2011), developed by the NMFS Northwest Region. The criteria applicable to the sizing and design of new screening facilities for the project include the following:

- Maximum approach velocity: 0.4 fps (assumes an active screen)
- Effective screen area: maximum screen flow/allowable approach velocity
- Submergence: 65% to 85% of drum diameter (for rotating drum screens)
- Sweeping velocity: 0.8 to 3.0 fps
- Screen material: corrosion-resistant and sufficiently durable to maintain a smooth, uniform surface with long-term use
- Maximum opening size
  - 0.087 inch for woven wire mesh (6 to 14 mesh)
  - 1.75 millimeters for slotted screens
  - 3/32-inch-diameter for circular screen openings (includes perforated plate)
  - 3/32 inch on diagonal for square screen openings
- Minimum open area: 27%

The project will use an existing screen that WDFW has already fabricated and is storing at its screen shop in Yakima, Washington. The screen will meet all of these criteria.

## 4.3 Delivery Pipelines

Pipelines will replace two sections of open, unlined conveyance ditches and will be designed to convey water from the intake to earthen conveyance ditches closer to the points of use. The pipelines will generally be designed to flow partially full by gravity. However, the profile of the segment of pipeline that crosses Swauk Creek will need to rise and fall in elevation and will be designed to flow full. The following requirements and criteria apply to the design of these pipelines:

- **Sizing of Gravity Flow Pipelines:** Gravity pipelines will be designed to convey the full flow rate while flowing less than 75% full. Pipe will be sized to maximize velocities while ensuring that pipelines have adequate capacity and do not flow full.
- **Sizing of Closed Pipelines:** As a general guideline, closed pipelines will be sized to limit velocities to a maximum of 5 fps and to limit pressure loss.
- **Pipe Roughness:** For completing hydraulic analysis of the proposed delivery system, a Manning's formula roughness coefficient (n) of 0.012 was used to estimate hydraulic loss in each delivery pipeline, consistent with recommendations of HDPE pipe manufacturers.
- **Trenching and Backfill:** Where possible, delivery pipelines will be designed with a minimum burial cover of at least 30 inches. Imported bedding and select backfill will be used to provide a solid foundation and protection for the pipeline.

## 5 Design Analyses

This section summarizes the analyses completed to support the selection of a preferred design alternative and design of the project.

#### 5.1 Alternatives Considered

RCO Manual 18 provides guidance for funding of salmon recovery projects. Appendix D-2 of Manual 18 provides guidance for deliverables needed to demonstrate that salmon recovery funding goals are achieved by proposed design and construction projects. One of the key elements required for SRFB-funded projects is consideration and evaluation of alternatives to demonstrate that the design alternative selected provides the best overall solution for achieving stated salmon recovery project goals. The goals for this project, as stated in Section 1 of this report, include the following:

- Eliminate irrigation-related mortality of steelhead, coho, and Chinook salmon at Swauk Creek RM 7.71 and significantly reduce the irrigation-related mortality of steelhead, coho, and Chinook salmon at Swauk Creek RM 7.92.
- 2. Restore year-round fish passage for all life stages of salmonids at Swauk Creek RM 7.71 and RM 7.92.
- Improve summer rearing conditions for juvenile steelhead, coho, and Chinook salmon in Swauk Creek by increasing irrigation efficiency, resulting in up to 0.25 cfs of conserved water (approximately 8% of the water right) available for instream flow benefits.
- 4. Increase canopy cover, provide shade, and produce a source of future large woody debris for Swauk Creek and its floodplain by planting up to approximately 3.5 acres with cottonwood copses.

An initial review of the preliminary design report for the project by the SRFB Review Panel identified the need to document the design alternatives considered and provide an evaluation of alternatives sufficient to demonstrate that the selected design alternative is the best overall option for meeting the salmon recovery goals of the project. This section of the report outlines the alternatives that were considered, describes the benefits and challenges of each alternative considered, documents why the preferred alternative was selected as the best option for meeting the goals of the project, and provides detailed analysis to support the design of the preferred alternative.

The following alternatives were considered by KCCD for improving fish passage and habitat conditions along Swauk Creek through the project reach:

Alternative 1 is the preferred alternative described in detail in this report. It would consolidate
the two gravity irrigation diversions on Swauk Creek at RM 7.92 and RM 7.71 to a single point of
diversion, at the location of the existing upstream point of diversion (RM 7.92). The diversion
facilities at RM 7.92 would be upgraded to handle the combined flow and address existing

deficiencies. Improvements would also be made to the roughened channel at that location. The fish screen and bypass pipeline would also be replaced. The diversion facilities at RM 7.71 would be removed and the left bank of the stream channel would be restored. Segments of open irrigation ditches would be piped to conserve water. Cottonwood copses would be planted to enhance the riparian area along the creek west of Burke Road.

- Alternative 2 would maintain and upgrade diversion facilities at both RM 7.92 and RM 7.71. The design of new diversion facilities would be completed with the intent of reducing the scale and impact of the facilities on the stream channel, while ensuring that the facilities have the capacity to divert the full water right at each point of diversion to The Ranch at Swauk Creek. Improvements would include roughening the channel or installing rock weirs to ensure sufficient water surface elevations exist in the stream channel to maintain diversions of up to 2 cfs at RM 7.92 and up to 1.5 cfs at RM 7.71 throughout the irrigation season. Screening and bypass facilities would be upgraded to address deficiencies. Segments of open irrigation ditches would be piped to conserve water. Cottonwood copses would be planted to enhance the riparian area along the creek west of Burke Road.
- Alternative 3 would consolidate the two gravity irrigation diversions on Swauk Creek at RM 7.92 and RM 7.71 to a single point of diversion at the location of the existing downstream point of diversion (RM 7.71). The diversion facilities at RM 7.71 would be upgraded to handle the combined flow and address existing deficiencies. Improvements would also be made to the stream channel at this location to ensure that the water surface elevations would be sufficient to maintain diversions. The fish screen and bypass would be replaced. The diversion at RM 7.92 would be removed and the right bank of the stream channel would be restored. Segments of open irrigation ditches would be piped to conserve water. Cottonwood copses would be planted to enhance the riparian area along the creek west of Burke Road.
- Alternative 4 would be similar to Alternative 1, with the following variations:
  - Rather than installing a piped fish bypass to return fish from the screen to Swauk Creek, an open channel would be constructed to allow fish bypass/return at the point of diversion.
  - Rather than replacing open segments of ditch with buried pipelines, portions of the canal system would be selectively lined or partially piped to avoid removing native trees and shrubs and small patches of cattails near or within the existing irrigation ditch on the right bank of Swauk Creek.

Each of these alternatives would be designed and constructed to minimize or avoid dewatering of the stream channel and remove barriers to fish passage in Swauk Creek. For each alternative, the fish screen replacements and diversion facilities would be designed to minimize the size and impact of these facilities.

#### 5.2 Alternatives Evaluation and Comparison

The alternatives were evaluated and compared to select a preferred alternative for design. Table 5-1 summarizes the key characteristics, challenges, and constraints associated with each alternative. Alternative 1 was selected as the preferred alternative based on evaluation and comparison of these key characteristics, challenges, and constraints. The following provides key conclusions from the evaluation that demonstrate why Alternative 1 was selected as the preferred design alternative:

- The invert elevation of the inlet to the diversion pipeline (2,178.8 feet) at the lower diversion (RM 7.71) is substantially higher than the invert of the stream channel adjacent to the diversion. Consequently, under low flow conditions, the ranch operator installs temporary pipe to extend the inlet up the channel to a location where the water surface elevation can be elevated to consistently divert water into the pipeline.
- The lower diversion (RM 7.71) is lower than the invert of the canal that delivers water from the upper diversion to the pasture north and west of Swauk Creek. The invert of the diversion pipeline is 2,178.8 feet and the invert of the culvert on the irrigation canal at Burke Road on the north side of Swauk Creek is just under 2,183.9 feet. Consequently, Alternative 3, which proposes to consolidate diversions at the location of the lower diversion, would not be feasible without pumping.
- The channel is steep both upstream and downstream of the lower diversion. Establishing stream conditions at the lower point of diversion that would be suitable for diverting water would require more extensive in-channel work than would be needed at the upper diversion location.
- The potential for fish to be entrapped in the existing lower diversion facilities is very high. The screening location is far (approximately 500 feet) downstream of the point of diversion at the left bank of Swauk Creek, and fish are easily entrapped in the diversion pipe and ditch segments between the creek and the fish screen.
- Fish that are entrained in the ditch will often remain in the ditch when irrigation water is shut off and can be left stranded in the segments of pipe and ditch between the creek and the fish screen, resulting in fish mortality.
- The upper diversion (RM 7.92) includes facilities that are much more consolidated, easier to access, and offer less opportunity for fish entrapment, injury, and mortality.
- The fish screen at the lower diversion does not function well and does not meet current WDFW
  and NMFS fish screening criteria. The screen is not as accessible as the upstream screen, and so it
  cannot be as easily adjusted to address problems that occur. The fish screen experiences
  inadequate sweeping velocity and overtops under high flow conditions.

Table 5-1 Comparison of Alternatives

Key Design Characteristic	Alternative 1	Alternative 2	Alternative 3	Alternative 4
Proposed Improvements:				
Diversion at RM 7.92	Diversions to be consolidated at RM 7.92.  Diversion to be upgraded to deliver 3.5 cfs without placing plastic and other materials in the creek.	Diversion to be upgraded so that full water right (2 cfs) can be diverted without placing plastic and other materials in the creek.	Diversion to be removed.	Diversions to be consolidated at RM 7.92. Diversion to be upgraded to deliver 3.5 cfs without placing plastic and other materials in the creek.
Diversion at RM 7.71	Diversion to be removed.	Diversion to be upgraded so that full water right (1.5 cfs) can be diverted without placing plastic and other materials in the creek.	Diversions to be consolidated at RM 7.71.  Diversion to be upgraded to deliver 3.5 cfs without placing plastic and other materials in the creek.	Diversion to be removed.
In Channel	Install boulders and cobbles to create roughened channel rock ramp downstream of diversion at RM 7.92. No revisions to channel near diversion at RM 7.71.	Install boulders and cobbles to create roughened channel rock ramp downstream of diversion at RM 7.92. Install boulders and cobbles to create roughened channel from upstream of diversion at RM 7.71 downstream to US Highway 97 bridge.	No revisions to channel near diversion at RM 7.92. Install boulders and cobbles to create roughened channel from upstream of diversion at RM 7.71 downstream to US Highway 97 bridge.	Install boulders and cobbles to create roughened channel rock ramp downstream of diversion at RM 7.92.
Fish Screening	New rotating drum fish screen to be installed near RM 7.92.	New rotating drum fish screen to be installed near RM 7.92.	Fish screen on upper diversion system to be removed or abandoned.	New rotating drum fish screen to be installed near RM 7.92.
	Fish screen on lower diversion system to be abandoned.	New fish screen to be installed closer to point of diversion at RM 7.71.	New fish screen to be installed closer to point of diversion at RM 7.71.	Fish screen on lower diversion system to be abandoned.

Key Design Characteristic	Alternative 1	Alternative 2	Alternative 3	Alternative 4
Bypass	New bypass pipe to be installed from new fish screen near RM 7.92 to pool upstream of boulder on right bank of creek. Existing bypass pipe from screen on lower diversion to be removed or abandoned.	New bypass pipe to be installed from new fish screen near RM 7.92 to pool upstream of boulder on right bank of creek. Existing bypass pipe from screen on lower diversion to be abandoned. New bypass pipe to be installed from new fish screen location near RM 7.71.	Existing bypass pipe from screen on upper diversion to be removed or abandoned. Existing bypass pipe from screen on lower diversion to be removed or abandoned. New bypass pipe to be installed from new fish screen location near RM 7.71.	New bypass channel (open channel) to be installed from new fish screen near RM 7.92 to pool upstream of boulder on right bank of creek. Existing bypass pipe from screen on lower diversion to be removed or abandoned.
Irrigation Conveyance	Open ditches to be replaced with buried pipelines.	Open ditches to be replaced with buried pipelines.	Open ditches to be replaced with buried pipelines.	Open ditches to be partially lined or partially piped to preserve key riparian plants along ditch bank.
Challenges and Constraints:				
Diversion at RM 7.92	In-channel improvements would be needed to maintain diversion of 3.5 cfs.  Improvements need to consider potential for flooding upstream.	In-channel improvements would be needed to maintain diversion of 2.0 cfs. Improvements need to consider potential for flooding upstream.	The existing diversion structure and headgate would need to be removed.	In-channel improvements would be needed to maintain diversion of 3.5 cfs. Improvements need to consider potential for flooding upstream.

Key Design Characteristic	Alternative 1	Alternative 2	Alternative 3	Alternative 4
Diversion at RM 7.71	The diversion is less accessible.	The diversion is less accessible.	The diversion is less accessible.	The diversion is less accessible.
	Approximately 500 feet of diversion pipeline and ditch between the point of diversion and the fish screen is not screened. Fish entrainment in the diversion facilities is a problem. Existing diversion facilities would need to be removed or abandoned.	Approximately 500 feet of diversion pipeline and ditch between the point of diversion and the fish screen is not screened. Fish entrainment in the diversion facilities is a problem.  The diversion pipe inlet is high relative to the invert of the existing creek at RM 7.71.	Approximately 500 feet of diversion pipeline and ditch between the point of diversion and the fish screen is not screened. Fish entrainment in the diversion facilities is a problem.  The diversion pipe inlet is high relative to the invert of the existing creek at RM 7.71.	Approximately 500 feet of diversion pipeline and ditch between the point of diversion and the fish screer is not screened. Fish entrainment in the diversior facilities is a problem. Existing diversion facilities would need to be removed or abandoned.
	of abandoned.	In-channel improvements would be needed to maintain diversion of 1.5 cfs. Improvements need to consider impact to US Highway 97 bridge.	Diversion elevations are not high enough to deliver water by gravity to pasture on the north side of Swauk Creek.  Replacement of the diversion structure and pipeline would be needed to increase capacity to 3.5 cfs.	of availabled.
			In-channel improvements would be needed to maintain diversion of 3.5 cfs.	
			Improvements need to consider impact to US Highway 97 bridge.	

Key Design Characteristic	Alternative 1	Alternative 2	Alternative 3	Alternative 4
In Channel	Plastic draped over a metal rod is installed in the channel to maintain diversions at RM 7.92 in the late summer. It is a barrier to fish passage. In-channel improvements would be needed.  Cattle rail with plastic draped over it and temporary pipe are installed to maintain diversions at RM 7.71. It is a barrier to fish passage. The diversion would be removed or abandoned.	Plastic draped over a metal rod is installed in the channel to maintain diversions at RM 7.92 in the late summer. It is a barrier to fish passage. In-channel improvements would be needed.  Cattle rail with plastic draped over it and temporary pipe are installed to maintain diversions at RM 7.71. It is a barrier to fish passage. In-channel improvements would be needed.	Plastic draped over a metal rod is installed in the channel to maintain diversions at RM 7.92 in the late summer. It is a barrier to fish passage. The diversion would be removed or abandoned. Cattle rail with plastic draped over it and temporary pipe are installed to maintain diversions at RM 7.71. It is a barrier to fish passage. The diversion would be removed or abandoned.	Plastic draped over a metal rod is installed in the channel to maintain diversions at RM 7.92 in the late summer. It is a barrier to fish passage. In-channel improvements would be needed. Cattle rail with plastic draped over it and temporary pipe are installed to maintain diversions at RM 7.71. It is a barrier to fish passage. The diversion would be removed or abandoned.
Fish Screening	The existing fish screen at RM 7.92 is only sized for a diversion of 2.0 cfs. A new screen would be needed. Hydraulic conditions at the fish screen do not maintain sweeping velocities and the screen requires a lot of cleaning and maintenance. The existing fish screen for the diversion at RM 7.71 would be removed or abandoned.	Hydraulic conditions at the fish screen at RM 7.92 do not maintain sweeping velocities and the screen requires a lot of cleaning and maintenance. A new screen would be needed.  The existing fish screen for the diversion at RM 7.71 is less accessible, too far (~500 feet) from the point of diversion; hydraulic conditions do not maintain appropriate sweeping velocities, and the screen is overtopped multiple times each season. A new screen would be needed closer to the point of diversion.	The existing fish screen for the diversion at RM 7.92 would be removed or abandoned.  The existing fish screen for the diversion at RM 7.71 is only sized for a diversion of 1.5 cfs, is less accessible, and is too far (~500 feet) from the point of diversion.  Hydraulic conditions do not maintain appropriate sweeping velocities, and the screen is overtopped multiple times each season. A new screen would be needed closer to the point of diversion.	The existing fish screen at RM 7.92 is only sized for a diversion of 2.0 cfs. A new screen would be needed. Hydraulic conditions at the fish screen do not maintain sweeping velocities and the screen requires a lot of cleaning and maintenance. The existing fish screen for the diversion at RM 7.71 would be removed or abandoned.

Key Design Characteristic	Alternative 1	Alternative 2	Alternative 3	Alternative 4
Bypass	The existing fish bypass pipe outlet from the diversion at RM 7.92 frequently becomes buried in the creek bank. It would need to be relocated. The existing fish bypass pipe outlet from the diversion at RM 7.71 is perched 3 feet above a rocky bank with no plunge pool below. It would be removed or abandoned.	The existing fish bypass pipe outlet from the diversion at RM 7.92 frequently becomes buried in the creek bank. It would need to be relocated. The existing fish bypass pipe outlet from the diversion at RM 7.71 is perched 3 feet above a rocky bank with no plunge pool below. It would need to be relocated with the screen.	The existing fish bypass pipe outlet from the diversion at RM 7.92 frequently becomes buried in the creek bank. It would be removed or abandoned.  The existing fish bypass pipe outlet from the diversion at RM 7.71 is perched 3 feet above a rocky bank with no plunge pool below. It would need to be relocated with the screen.	The existing fish bypass pipe outlet from the diversion at RM 7.92 frequently becomes buried in the creek bank. It would need to be relocated. The existing fish bypass pipe outlet from the diversion at RM 7.71 is perched 3 feet above a rocky bank with no plunge pool below. It would need to be relocated with the screen.
Irrigation Conveyance	The existing ditch on the right bank, supplied by the diversion at RM 7.92, is constructed in permeable alluvial material.	The existing ditch on the right bank, supplied by the diversion at RM 7.92, is constructed in permeable alluvial material.	The existing ditch on the right bank, supplied by the diversion at RM 7.92, is constructed in permeable alluvial material.	The existing ditch on the right bank, supplied by the diversion at RM 7.92, is constructed in permeable alluvial material.
	The existing pipeline and ditch on the left bank, supplied by diversion at RM 7.71, is also constructed in alluvial material, is less accessible, and is not on property owned by the ranch.	The existing pipeline and ditch on the left bank, supplied by diversion at RM 7.71, is also constructed in alluvial material, is less accessible, and is not on property owned by the ranch.	The existing pipeline and ditch on the left bank, supplied by diversion at RM 7.71, is also constructed in alluvial material, is less accessible, and is not on property owned by the ranch.	The existing pipeline and ditch on left bank, supplied by diversion at RM 7.71, is also constructed in alluvial material, is less accessible, and is not on property owned by the ranch.

- The fish bypass at the lower diversion does not function well and does not meet current WDFW NMFS guidelines. The bypass has been blocked at times to keep the screen functioning and delivering the flow rate needed by the ranch. The outlet of the fish bypass is perched 3 feet above the rocky bank of Swauk Creek with no plunge pool to safely return fish to the creek, causing injury and mortality to fish.
- The lower diversion, pipeline, ditch, fish screen, and bypass are not located on The Ranch at Swauk Creek property and access to the facilities is much more challenging.
- The lower point of diversion is just upstream of the U.S. Highway 97 bridge. The work required in the Swauk Creek channel to make the diversion reliable and operable without deploying barriers to the stream channel each summer could adversely affect the bridge structure downstream and would require additional analysis and potentially additional work at the bridge.
- Consolidating the irrigation points of diversion at the upper diversion location (RM 7.92) would eliminate a significant source of fish entrainment, injury, and mortality.
- Constructing an open channel bypass at the upstream diversion (RM 7.92) would be challenging due to the topography along the right bank of the creek. The channel would have to be relatively deep with a very gentle slope. Under high flows, water could back up into the diversion channel, and under peak flow conditions, the water surface would overtop the right bank and there would be risk of washing out the narrow bank that would remain between the fish bypass channel and the creek. A buried, piped bypass would reduce the risk of damage at high flows.
- Selectively lining and/or partially piping the canal, rather than fully replacing the open irrigation
  canal on the right bank of the creek with piping, may be feasible for the sake of preserving
  riparian vegetation that has developed adjacent to the canal. However, the following are benefits
  for replacing the canal with pipe:
  - The material between Swauk Creek and the irrigation canal is generally coarse, highly
    permeable alluvial sands, gravels, and cobbles. Consequently, groundwater levels generally
    correspond closely with creek levels and groundwater is relatively shallow, especially when
    the creek levels are high.
  - It is unlikely that groundwater levels adjacent to the canal are wholly influenced by the canal alone, but are also hydraulically connected to the adjacent creek.
  - In the late part of the irrigation season, when creek levels are low, it has become extremely
    difficult to divert water to the irrigation canal and keep enough flow in the canal for
    irrigation.
  - In the early part of the irrigation season, when the creek is high, the canal can also gain water via high groundwater that seeps into the canal from the creek.
- Based on these considerations, KCCD recommended piping the canal to potentially conserve up
  to 0.25 cfs by reducing seepage. KCCD determined that the water conservation savings would be
  worth the potential risk to riparian vegetation. The conserved water would reduce the amount
  diverted, providing a flow benefit to the creek. Final calculations of conserved water that would

result from converting the open ditch to a pipeline for delivery will be completed after additional assessment (continued flow measurement and potential the use of the U.S. Department of Agriculture Natural Resources Conservation Service ditch loss calculator).

Overall, resolving the issues at the lower point of diversion would require a complete reconfiguration of the diversion system, which would require much more effort and cost. As a result, Alternatives 2 and 3, which would require continued use of the lower diversion at RM 7.71, were not selected as the preferred alternative.

Providing an open bypass canal, which was identified as part of Alternative 4, would expose the right bank to potential damage and washout at the diversion under high flow conditions and was not considered a preferred option. Likewise, lining or partial piping of the irrigation ditch was considered feasible but would not provide the same level of conservation savings as replacing the irrigation ditch with piping and was not recommended as a preferred option.

Based on this analysis and comparison of potential alternatives, Alternative 1 was identified as the preferred alternative and best option for meeting the salmon recovery goals for the project and improving the operation of the irrigation system that serves The Ranch at Swauk Creek.

## 5.3 Hydrologic Analysis

The hydrology of Swauk Creek was evaluated to determine likely flow conditions at the project site. To the extent possible, the project will be designed to maintain diversions throughout the irrigation season and provide fish passage during critical migratory periods for key fish species. This section provides a summary of that analysis.

## 5.3.1 Existing Flow Data

The Swauk Creek watershed drains approximately 83 square miles upstream of the project site and is predominately a snowmelt-dominated system. The U.S. Geological Survey (USGS) StreamStats (USGS 2020) program estimates that the mean annual precipitation in the watershed is approximately 27 inches per year, but precipitation varies widely throughout the watershed, depending on location and elevation. Flows in the creek are continuously monitored at the following location:

• Ecology Gage No. 39M130, Swauk Creek Below First Creek: This gage is located approximately 0.5 mile northeast of the intersection of U.S. Highways 97 and 970 at latitude 47°12′30", longitude 120°42′2", approximately 0.4 mile upstream from the proposed project site. Flows have been monitored at this location since May 2014.

#### 5.3.2 Annual Variation in Flow Rates

Peak flows in Swauk Creek typically correspond with winter and spring storm events and snowmelt. Because peak flows occur outside the irrigation season, it is unlikely that diversions have a significant impact on peak streamflow rates measured at the gage on Swauk Creek.

The peak 15-minute flow rates measured on Swauk Creek at Ecology Gage No. 39M130 were 498 cfs (recorded December 10, 2015; February 15, 17, and 18, 2016). Because the period of flow measurement covers only 6 years, a precise estimate of the 100-year flood flow rate cannot be made from the data available. The StreamStats program estimates the 100-year flow at 1,180 cfs. Because a precise estimate of the 100-year flood flow rate could not be made from the gage data available, the StreamStats estimated 100-year flow was used as a peak flow rate for design of the proposed improvements.

Flow statistics for daily mean flows recorded at Ecology Gage No. 39M130 are plotted in Figure 5-1. The 10%, 50%, and 90% daily mean exceedance values are plotted to show the variability of flows throughout the year. The 10% exceedance values represent wet conditions, the 90% exceedance values represent dry conditions, and the 50% exceedance values represent the median. These are plotted against the 10%, 50%, and 90% overall exceedance values for the full record of daily mean flows recorded at this gage.

Streamflow statistics are summarized in Table 5-2. As shown in Figure 5-1 and in Table 5-2, for wetter than normal years, flows at the Ecology gage are typically greater than 3.0 cfs throughout the irrigation season. However, daily mean flows measured at the Ecology gage typically drop below 3.0 cfs during the late summer in normal to drier than normal years.

WDFW fish passage design guidance (WDFW 2013) indicates that the high design flow should be the 10% exceedance flow for the month(s) of migration for the species of interest, in this case summer steelhead. From data on adult fish tracking in Swauk Creek, April sees the majority of adult steelhead passing through the system. The 10% exceedance flow for April is 264 cfs. For the low-flow design, WDFW (2013) recommends using either the 2-year, 7-day low flow, or a zero flow. However, the 80% exceedance flow was chosen because it is a very low flow when accounting for irrigation withdrawals of up to 3.5 cfs. As an illustration, the 90% exceedance flow of 3.2 cfs is less than the water right.

Low flows naturally occur during the late summer and early fall, when irrigation demand is the highest. Table 5-3 summarizes average late-summer 2-week average flow rates in Swauk Creek, based on the flows measured at Ecology Gage No. 39M130. The data indicate that flows in late August and early September may be less than the total 3.5 cfs surface water right at The Ranch at Swauk Creek, which suggests that during the late summer, the ranch may not be able to fulfill its water right. A detailed trust water right analysis, as summarized following Table 5-3, was completed

by KCCD as part of this study to demonstrate that the probability of dewatering the creek at the proposed diversion is very low.

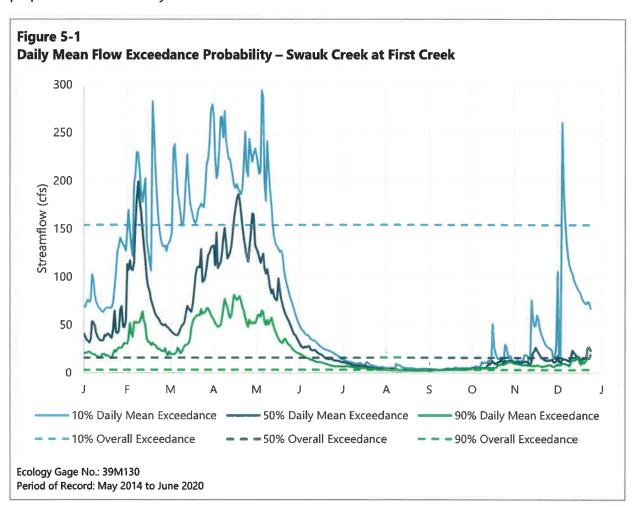


Table 5-2
Swauk Creek Streamflow Statistics

	Streamflow (cfs)								
Parameter	2014 (Partial)	2015	2016	2017	2018	2019	2020 (Partial)	All Years	
Maximum	227	236	498	311	411	255	99.8	498	
Minimum	3.0	1.6	1.6	2.3	1.7	1.4	2.6	1.4	
Average	34.9	33.9	80.5	62.6	53.8	28.9	33.3	48.8	

19 4	Streamflow (cfs)								
Parameter	2014 (Partial)	2015	2016	2017	2018	2019	2020 (Partial)	All Years	
10% Exceedance	125	120	210	213	191	101	162	154	
90% Exceedance	3.9	5.2	3.2	3.0	3.0	3.6	3.1	3.2	

Note: Streamflow data from Ecology Gage No. 39M130

Table 5-3
Summary of Irrigation Season 2-Week Flow Rates

Date Range	Average Flow (cfs)
April 1 to April 15	145.9
April 15 to April 30	141.7
May 1 to May 15	133.8
May 15 to May 31	76.8
June 1 to June 15	31.0
June 15 to June 30	18.1
July 1 to July 15	10.0
July 15 to July 31	6.4
August 1 to August 15	4.2
August 15 to August 31	3.3
September 1 to September 15	3.1
September 15 to September 30	3.8

Note: Streamflow data from Ecology Gage No. 39M130

## 5.3.3 Trust Water Right Analysis

A trust water right analysis was completed by KCCD to more closely evaluate water availability for both irrigation and maintaining instream flows below the proposed consolidated diversion for The Ranch at Swauk Creek at RM 7.92. That analysis is included in Appendix C.

In addition to the irrigation diversions on Swauk Creek,, another irrigation diversion was located at RM 3.9 on First Creek, which is a left-bank tributary that joins Swauk Creek at RM 8.4, upstream of The Ranch at Swauk Creek. The water right on First Creek has the senior water right in the watershed, with a priority date of 1877. The water rights for The Ranch at Swauk Creek are next in priority, with a priority date of 1878. Portions of these water rights have since been put into trust to maintain instream flows. Trust water quantities associated with these diversions restrict the quantity of water that can be diverted for irrigation depending on the flow conditions in First Creek and Swauk Creek.

Trust water right quantities associated with the water rights on First Creek and on Swauk Creek at The Ranch on Swauk Creek vary based on the month of the irrigation season. The quantity of trust water on First Creek is established at the point of diversion at RM 3.9 on First Creek and is expected to remain as instream flow in First Creek and downstream in Swauk Creek, beyond the diversions at either RM 7.92 or RM 7.71. The quantity of trust water in First Creek may be adjusted if the flow from First Creek to Swauk Creek, as measured at the mount of First Creek, is below the trust water quantity. The quantity of water diverted to The Ranch at Swauk Creek is also subject to a trust water right on Swauk Creek.

Due to natural fluctuations in flows in First and Swauk Creeks, trust water quantities and the quantity of water available for irrigation diversions are typically impacted most frequently during the mid to late summer months, when natural flows are lowest. During low flow conditions, when flows in First Creek and Swauk Creek are less than the combined trust water and irrigation water rights, the following adjustments are made:

- The trust water quantity in First Creek is reduced to the flow rate measured at the mouth.
- The flow rate measured at the mouth of First Creek (the trust water quantity) is expected to pass
   The Ranch at Swauk Creek diversion at RM 7.92 and continue down Swauk Creek.
- The flow in Swauk Creek is reduced by the trust water quantity from First Creek and then prorated based on the trust water quantity for Swauk Creek, which is a percentage of the total water right on Swauk Creek. For example, in August, the flow measured at the mouth of First Creek would be subtracted from the total flow in Swauk Creek as the instream quantity for First Creek. The remaining flow would be multiplied by 89.74% to accommodate the trust water quantity associated with the water right on Swauk Creek. The resulting flow would be available for diversion to The Ranch at Swauk Creek.

KCCD completed an analysis of flow rates recorded at the Ecology flow monitoring gage on Swauk Creek to determine what quantities of water would have been available for irrigation diversion to The Ranch at Swauk Creek and what flow rates would have been passed downstream as instream flows through the period of historical flow record. The results indicate that the reach of Swauk Creek downstream of the diversion would not have been dewatered during this period. Flows downstream of the diversions to The Ranch at Swauk Creek would have dropped to approximately 0.92 cfs in the summer of 2018. Flows available for diversion to the ranch would have dropped to 2.1 cfs late in the summer of 2018.

## 5.4 Hydraulic Analysis

## 5.4.1 Intake Hydraulics

Existing and proposed stream channel conditions were modeled using the U.S. Army Corps of Engineers (USACE) Hydrologic Modeling System software one-dimensional hydraulic model (HEC-RAS; USACE 2017) to determine velocities, flow depths, and shear stresses on the channel and to compare existing and proposed channel conditions. The following topographic data were used for modeling existing conditions:

- Surveyed Topography (2020): As part of this project, KCCD subcontracted with HLA Engineering and Land Surveying, Inc., to collect topographic data of the creek, diversion ditch, intake facilities, and adjacent upland areas.
- **LiDAR Data:** For areas beyond the extents of these two datasets, contours generated from LiDAR data from the Washington Department of Natural Resources LiDAR Portal were incorporated into the surface to complete the topography.

The proposed design contours and channel sections were used to modify existing channel sections, and to model proposed conditions. The existing conditions and alternatives were modeled using the following design flow conditions:

- Q<sub>low</sub> = 4.6 cfs (80% overall exceedance flow)
- Qhigh = 264 cfs (10% exceedance flow during April steelhead migratory season)
- Q<sub>2-year</sub> = 356 cfs (channel-forming flow to inform the design of channel restoration elements)
- Q<sub>100-year</sub> = 1,180 cfs (peak flow to ensure stability of design elements)

A Manning's roughness coefficient (n) of 0.045 was used to model all but the low-flow condition. Given the depth of flow relative to the rock size during the low-flow condition, a much higher n value of 0.25 was used. The low-flow roughness coefficient was selected based on guidance in the U.S. Forest Service technical report *Photographic Guidance for Selecting Flow Resistance Coefficients in High-Gradient Channels* (Yochum 2014).

The 2-year flow was included as the channel-forming flow, during which velocities and shear stresses will have a high impact on the geomorphic response of the channel. The 100-year flow estimated by the StreamStats program was modeled to evaluate channel stability under peak flow conditions.

Table 5-4 summarizes the average channel velocities at key cross sections for both existing and proposed conditions at the 100-year, 2-year, 10% April exceedance, and 80% overall exceedance flows. More detailed HEC-RAS results are included as Appendix D.

Table 5-4
Summary of Hydraulic Analysis Results at Key Sections

Channel Cross Section Location Relative to Intake	Model Station (feet)	Channel Manning's Roughness (n) Used	Flow	Average Velocity, Existing Conditions (fps)	Average Velocity, Proposed Conditions (fps)
		0.045	100-Year	11.36	11.60
104 for at 100 atmosphere	F0C0 13	0.045	2-Year	7.40	7.35
104 feet upstream	5069.13	0.045	April 10% Exceedance	6.36	6.27
		0.25	80% Exceedance	0.31	0.33
		0.045	100-Year	9.73	7.39
70 (	5042.00	0.045	2-Year	6.91	5.37
79 feet upstream	5043.89	0.045	10% Exceedance (April)	6.03	4.95
		0.25	80% Exceedance	0.34	0.73
		0.045	100-Year	9.61	5.94
22.5	4997.51	0.045	2-Year	6.8	3.03
32 feet upstream		0.045	10% Exceedance (April)	6.17	2.56
		0.25	80% Exceedance	2.26	0.11
	4965.06	0.045	100-Year	8.11	9.27
		0.045	2-Year	5.21	4.51
Intake		0.045	10% Exceedance (April)	4.74	4.14
		0.25	80% Exceedance	0.35	0.45
	4943.60	0.045	100-Year	6.16	7.01
		0.045	2-Year	4.51	6.68
21 feet downstream		0.045	10% Exceedance (April)	3.93	5.89
		0.25	80% Exceedance	0.22	0.54
		0.045	100-Year	6.65	8.83
F7 ( d	4000.00	0.045	2-Year	4.8	6.56
57 feet downstream	4908.09	0.045	10% Exceedance (April)	4.46	5.75
		0.25	80% Exceedance	0.34	0.81
		0.045	100-Year	6.27	7.11
0.4.6	4074.20	0.045	2-Year	4.18	4.84
94 feet downstream	4871.20	0.045	10% Exceedance (April)	3.86	4.59
		0.25	80% Exceedance	0.41	0.47

Channel Cross Section Location Relative to Intake	Model Station (feet)	Channel Manning's Roughness (n) Used	Flow	Average Velocity, Existing Conditions (fps)	Average Velocity, Proposed Conditions (fps)
118 feet downstream	4847.25	0.045	100-Year	4.12	4.95
		0.045	2-Year	2.73	3.24
		0.045	10% Exceedance (April)	2.47	3.00
		0.25	80% Exceedance	0.17	0.24

#### Notes:

- 1. The 100-year flow was 1,180 cfs
- 2. The 2-year flow was 356 cfs
- 3. The 10% exceedance flow for April was 264 cfs
- 4. The 80% overall exceedance flow is 4.6 cfs.

Potential changes in average channel velocity were estimated between existing and proposed conditions during the 10% April and 80% low flows (fish passage design flows) to identify fish passability of the proposed roughened channel. For the most part, velocities upstream of the diversion are slightly lower for the proposed condition under the 10% exceedance flows and slightly higher for the 80% exceedance flows. Velocities downstream of the intake along the roughened channel are estimated to be higher under the proposed conditions, with average velocities along the roughened channel for the 10% exceedance flows ranging from 3.0 to 5.9 fps. WDFW guidance recommends that the average flow velocities in the channel during migration should not exceed 4 fps for culverts and other crossings (WDFW 2013). The estimated velocities under the proposed conditions exceed this value; however, they are similar to velocities in the creek channel both upstream and downstream of the roughened channel and are well within the swimming capabilities of both adult steelhead and coho salmon that can swim at sustained speeds of 4 to 10 fps (Bell 1991). During the low design flow, average velocities are below 1 fps. Because the roughened channel will have large rock spaced throughout the ramp that would create hydraulic shadows (lowvelocity areas behind the rocks), it is likely that juvenile fish would be able to pass upstream during low flows.

Potential changes in velocity were also compared for existing and proposed conditions at the 2-year flow event and the 100-year flow event (Table 5-4). These flows both contribute to channel-forming and geomorphic processes, but fish would not likely be attempting to migrate upstream during these peak flows. The velocities during the 100-year event are additionally important for channel stability, and the proposed design generally shows similar velocities overall, with some cross sections showing higher velocities and some showing lower velocities. The sections showing a reduction in the 100-year velocities indicate that channel stability will improve once the project is constructed. Sections showing increased velocities are mainly along the roughened channel which was designed to withstand higher velocities.

The HEC-RAS model indicates that under the modeled 100-year flow conditions, the water surface in the creek would overtop the intake structure by almost 1 foot. Flow conditions approaching the 1,180-cfs flow modeled as the 100-year flow were not observed in the period of record at Ecology Gage No. 39M130. The highest flow recorded at the gage was 498 cfs during the winter of 2015 to 2016. The model indicates the water surface in the creek would overtop the intake structure by approximately 0.3 foot at this flow rate. We are not aware of conditions that were observed during this event, but the aerial photographs indicate that the stream has shifted course upstream of the intake location over the last 10 years. Table 5-5 summarizes the water surface elevations calculated in the model for the 100-year flow conditions near the intake. The greatest increase in water surface elevation occurs nearest the intake structure. The modeled 100-year water surface elevation does not appear to impact any houses or other structures and is likely similar to the conditions before the previous rock ramp shifted.

Table 5-5
Modeled 100-Year Water Surface Elevations at Key Sections

Channel Cross Section Location Relative to Intake	Model Station (feet)	Water Surface Elevation, Existing Conditions (ft)	Water Surface Elevation, Proposed Conditions (ft)	Difference (ft) [Proposed]-[Existing]
104 feet upstream	5069.13	2196.22	2196.19	-0.03
79 feet upstream	5043.89	2195.84	2196.56	0.72
32 feet upstream	4997.51	2194.88	2196.44	1.56
Intake	4965.06	2194.67	2195.46	0.79
21 feet downstream	4943.60	2194.76	2195.42	0.66
57 feet downstream	4908.09	2194.34	2194.39	0.05
94 feet downstream	4871.20	2194.18	2193.62	-0.56
118 feet downstream	4847.25	2194.30	2193.77	-0.53

#### 5.4.2 Fish Screen Analysis

As noted in Section 4.2, fish screening facilities will need to be designed to meet the most current requirements for screening of diversions from the WDFW and NMFS *Anadromous Salmonid Passage Facility Design Guidelines* (NMFS 2011). Based on discussions with KCCD and WDFW, it is proposed that a modular rotating drum screen that has already been fabricated by WDFW and is being stored at WDFW's Yakima Screen Shop will be used for this project. Information about the proposed fish screen to be used for this project is included in Appendix E.

It is our understanding that WDFW will furnish and deliver the rotating drum screen and will assist with installation in generally the same location as the existing screen. The project contractor will be required to perform the earthwork needed to accommodate the new screen, and to place and

compact foundation material for the screen. The screen is a 24-inch-diameter, 6-foot-long modular rotating drum screen and has been designed by WDFW for a maximum flow rate of approximately 3.6 cfs. For the screen to operate properly, the hydraulic conditions need to maintain proper submergence, which means that the screen needs to stay 65% to 85% submerged relative to the height of the screen while in operation.

#### 5.4.3 Hydraulic Analysis of Delivery Pipeline

Hydraulic calculations were also completed to support the sizing and design of the delivery pipelines proposed to replace open gravity ditches. Gravity pipelines were evaluated using a backwater spreadsheet model that calculates hydraulic losses in a pipeline based on Manning's equation. The calculations also estimate velocities and the profile of the water surface in the pipeline. The calculations assume smooth-walled CPE pipe with a Manning's n value of 0.012 for delivery pipelines that will operate partially full under gravity flow conditions. For delivery pipelines that run full, the analysis assumed that butt-fused, solid-wall HDPE pipe would be used, also with an n value of 0.012. These calculations are included as Appendix F.

The proposed pipeline will mostly operate as gravity flow, running partially full. Pipeline segments have been designed so that pipelines will flow generally less than 75% full under design flow conditions. These segments of pipeline will be watertight CPE pipe. The segment of pipeline that extends south from Ranch Road along the south side of Burke Road will have a profile with low points and high points, as required to cross the bridge over Swauk Creek and maintain appropriate depths of cover elsewhere. This segment of pipe will be designed to run full by filling the upstream manhole to an elevation that is above the crown of the pipe and discharging to a downstream manhole that is full above the elevation of the crown of the pipe. Because this segment of pipe will run full, it will need to be designed to accommodate low pressures, so solid-wall, butt-fused HDPE pipe is recommended. Based on the results of the analysis, pipe sizes will vary from 10-inch diameter for the pipeline extending south along Burke Road to 15-inch diameter for the pipeline that conveys water from the intake facilities to the manhole at Burke Road.

## 5.5 Geology and Geomorphology

The geology of the watershed is predominantly Tertiary-era, nonmarine sedimentary rocks and basalts in the Swauk and Wenatchee Formations and related ash-flow tuffs, and Miocene-era basalt flows from the Columbia River basalts overlaying much older metamorphic schists. These layers were folded and uplifted as the Cascade Range rose and the Columbia Plateau subsided (Tabor et al. 1982). Surficial deposits include glacial morainal deposits and glacial till, particularly the deposits that created Swauk Prairie, which has two layers of glacial till with glacial lake deposits of clay and sand between the till layers. More recent alluvial deposits are present along Swauk Creek and from tributaries at deltaic fans.

The Soil Survey of Kittitas County Area, Washington (NRCS 2010) indicates that the predominant soils along the steeper upland slopes upstream of the project area include Sapkin-Rubble land complex (slopes 30% to 75%) that are derived from basalt and to a lesser extent loess (wind-blown glacial materials), and Keechelus gravelly ashy loam (slopes 30% to 60%) that are derived from basalt, brecchia, and pyroclastic rock with some volcanic ash in the upper part. Farther upstream in the watershed are complexes of Keechelus-Nard-Kafing soils. Nard soils are derived from sandstone and old alluvium with volcanic ash in the upper part. Kafing soils are derived from sandstone and siltstone with volcanic ash in the upper part. Kiper stony ashy sandy loams (slopes of 30% to 65%) are also present, derived from sandstone with volcanic ash in the upper part. There are numerous dredged placer mining spoils piles along the creek within the project area and for several miles upstream of the project area (see Figure 5-2).

In the floodplain of the project area, soils are primarily alluvial, including Quicksell loam (0% to 5% slopes); Patnish-Mippon-Myzel complex (0% to 3% slopes); and Teanaway ashy loam (3% to 10% slopes) derived from loess over glacial till with volcanic ash in the upper part.

Swauk Creek and its tributaries have cut their channels down through the glacial and bedrock materials, resulting in confined valleys until about RM 8 where Swauk Creek enters Swauk Prairie. In this area the creek was likely historically more complex with wetlands and a wide floodplain. Downstream of Swauk Prairie, the creek enters a confined valley as it approaches the Yakima River. Government Land Office mapping from 1892 (Figure 5-3) shows Swauk Creek with a slightly sinuous course and does not note wetlands or multiple channels. It is striking to see the number of mining claims and placer mining areas already in place by 1892.

Extensive mining, including placer mining in the creeks, has occurred in the watershed for over a century. Mining removed large wood and natural substrates and contributed to channel incision and confinement. Bedrock outcrops occur along the banks and bed of the creek in numerous locations (Figure 5-4). The construction of U.S. Highway 97 also straightened and channelized Swauk Creek in numerous locations. In Swauk Prairie, the creek has also likely been straightened along property lines, and beaver dams and riparian habitats have been removed. Interfluve (2010) estimated that an upstream reach of Swauk Creek was incised by 2.5 to 4 feet. Within the project area, the creek appears to have been excavated down at least 2 feet as evidenced by the dredged spoils piles adjacent to the creek.

The stream gradient through the project area is typically about 1.5%. The river substrates in the project reach are a mixture of gravel, cobbles, and some boulders and patches of sands and silts. The watershed has many natural sources of sediment that can be contributed via landslides, roads, and forestry or rural residential land uses (Figures 5-5 and 5-6). No substantial accumulations of sediment were noted in the creek channel in the vicinity of the irrigation diversion structures, although seasonal accumulation of sands and silts may occur in low-velocity areas. The fish bypass return pipe

downstream of the upper diversion becomes buried in sediment seasonally. Higher streamflows would transport gravels. Upstream of the upper diversion, the creek changed course and abandoned a meander bend during and after the high flows in 2009 (Figures 5-7, 5-8, and 5-9) as a result of gravel and debris deposition in the old channel.

Figure 5-2
Placer Mining Spoils Pile



Figure 5-4
Swauk Creek Confined Between Bedrock and Road Fill Near RM 10



Figure 5-5 Scree Slopes in Upstream Watershed



Figure 5-6
Siltstone in Upper Watershed

Figure 5-7
Swauk Creek Location in 2006 (Google Earth)



Figure 5-8
Swauk Creek Location in 2011 (Google Earth)



Figure 5-9
Swauk Creek in 2017 (Google Earth)

The Swauk Creek channel is fairly uniform in dimensions and gradient both upstream and downstream of the project reach, with bankfull dimensions ranging from 35 to 45 feet and slopes ranging from 1.5% to 2%. This is likely a legacy of the dredge mining that has generally confined the channel in its existing alignment and dimensions.

A roughened channel can accommodate passage of sediment and wood without changing its overall configuration because it generally replicates a natural slope and substrate conditions. It is likely that gravel will periodically accumulate near the diversion headgate structure (just upstream of the ramp), so gravel may need to be removed periodically, such as when the irrigation diversion is first opened each season.

The fish bypass return from the proposed screen would be located to discharge back into the creek further downstream of the existing bypass. The new alignment would discharge adjacent to a large rock and scour pool, reducing the potential for burial of the pipe outlet. The current bypass pipe discharges into a segment of the creek with the lowest gradient and most potential for sediment deposition.

## 6 Summary of Proposed Improvements

This section provides a detailed summary of the key facilities for the proposed project.

#### 6.1 Stream Channel Improvements

Stream channel improvements will include the construction of a roughened channel immediately downstream of the intake to create improved fish passage and ensure the adequate submergence depth of the fish screen and bypass facilities. The roughened channel will be created by placing 3-man to 5-man boulders immediately downstream of the intake to create a grade control. The roughened channel fishway will extend downstream at a 2.5% slope for 80 feet to meet a flatter section of the creek. The fishway will be composed of a well-graded gravel and cobble mix with boulders interspersed throughout. This slope is similar to the average slope along the entire creek. The roughened channel will include a low-flow channel designed to maintain depths and suitable velocity conditions during periods of low flows. The remainder of the channel was designed to withstand and pass the 100-year recurrence interval flow.

Bed material was sized using guidance in the U.S. Bureau of Reclamation Rock Ramp Design Guidelines (USBR 2007). Using methods cited in the guidelines, multiple sizing calculations were performed and the threshold shear stress required to move bed materials was calculated. The most conservative of these methods was used to decide on a median grain size ( $D_{50}$ ) of 18 inches. The guidance suggests using 1.5 times the  $D_{85}$  (85th percentile rock size) for the depth of the streambed material, which yielded a depth of approximately 42 inches.

The area near the downstream diversion to be removed will be graded, and the large boulders will be reworked to remove any drops larger than 6 inches. As necessary, the same gravel and cobble mix used upstream will be used to fill in void spaces in the boulders and minimize channel and bank erosion. The bank in the immediate vicinity of the removed diversion structure will be regraded, mixing in the gravel and cobble mix, then hydroseeded.

#### 6.2 Fish Screen Replacement

Fish screening facilities will be designed to meet the most current requirements for screening of diversions from WDFW and the NMFS *Anadromous Salmonid Passage Facility Design Guidelines* (NMFS 2008). Those criteria are outlined in Section 4.2. Based on discussions with KCCD and WDFW, it is proposed that a modular rotating drum fish screen will be used that has already been fabricated by WDFW and is being stored at their Yakima Screen Shop.

It is our understanding that WDFW has committed to furnish and deliver the rotating drum screen and will oversee installation of the screen. The screen will be installed at generally the same location as the existing screen. The project contractor will be required to perform the earthwork needed to

accommodate the new screen, and to place and compact foundation material for the screen. Key characteristics of the screen and recommended water surface elevations (WSELs) are as follows:

Screen diameter: 24 inches

Screen length: 6 feet

WDFW design flow rate: 3.6 cfs maximum

Screen bottom elevation: 2,190.27 feet (NAVD 88)

WSEL needed for 65% submergence: 2,191.57 feet (NAVD 88)

• WSEL needed for 70% submergence (target for design flow): 2,191.67 feet (NAVD 88)

WSEL needed for 85% submergence: 2,191.97 feet (NAVD 88)

For the screen to operate properly, the hydraulic conditions need to maintain proper submergence, which means that the screen needs to stay 65% to 85% submerged relative to the height of the screen while in operation. To ensure that the water surface is well within that targeted range, WDFW has recommended that the design target a submergence of 70% at the design flow of 3.5 cfs.

A new 8-inch solid-wall, butt-fused DR 32.5 HDPE fish bypass pipeline is recommended to replace the existing fish bypass. As noted earlier, the existing fish bypass pipeline outlets to a portion of the screen that accrues sediment and regularly becomes buried. Extending the outlet of the pipeline farther downstream, along with proposed channel improvements designed to maintain appropriate water levels at the screen, will allow for improved flow and outlet conditions through the fish bypass pipeline to ensure that the fish bypass pipeline does not backwater.

#### 6.3 Delivery Pipeline

Installation of the following segments of pipeline is recommended to replace open ditches and convey water from the intake facilities to points of delivery to The Ranch on Swauk Creek on both the north and south sides of Swauk Creek:

- Approximately 857 feet of 15-inch CPE pipe is recommended to convey 3.5 cfs from the intake facilities to the culvert under U.S. Highway 97.
- Approximately 364 feet of 15-inch CPE pipe is recommended to convey 3.5 cfs from the culvert under U.S. Highway 97 to a manhole near Burke Road where flows will be split.
- Approximately 10 feet of 12-inch CPE pipe is recommended to discharge up to 2.0 cfs from the manhole near Burke Road to the open ditch that extends west to irrigate pasture within the ranch north and west of Swauk Creek.
- Approximately 340 feet of 10-inch CPE pipe is recommended to convey up to 1.5 cfs along the south side of Burke Road from the first manhole to a second manhole near Ranch Road.
- The flow will fill the manhole at Ranch Road and the pipeline downstream of this manhole will operate completely full. Approximately 919 feet of 10-inch DR 32.5 solid-wall, butt-fused HDPE

- pipe is recommended to convey water from the manhole at Ranch Road across Swauk Creek to a manhole near the outlet to the open ditch south of Swauk Creek.
- Approximately 23 feet of 12-inch CPE pipe is recommended to discharge up to 1.5 cfs from the manhole south of Swauk Creek to the open ditch that conveys water to the pond on ranch property south and east of Swauk Creek.

#### 6.4 Riparian Plantings

Areas disturbed by the removal of the downstream irrigation diversion headwall and installation of the roughened channel areas will be graded to smooth slopes and seeded with native grass species (see Table 6-1) and red osier dogwood cuttings (*Cornus stolonifera*).

Table 6-1
Recommended Native Grass Seed Mix

Species Name	Common Name	Pounds/Acre
Agrostis idahoensis	ldaho redtop	3
Elymus glaucus	Blue wildrye	5
Elymus lanceolatus	Streambank wheatgrass	5
Festuca idahoensis	Idaho fescue	7

Downstream of the irrigation infrastructure improvements, approximately 3.5 acres of riparian habitat will be planted with cottonwood poles (*Populus balsamifera*) to supplement prior riparian plantings. Cottonwood poles should be 1.5 to 3 inches in diameter (butt end) and 8 to 12 feet in length, with all lateral branches cut off. Poles should be cut with a 45-degree angle on the butt end. The growing end should be cut flat and treated with tree paint or other suitable plant sealant to prevent desiccation. Poles should be harvested from within the watershed, kept in cold storage prior to delivery to the site, and then placed to soak the lower half for a minimum of 24 hours prior to planting. Cottonwood poles should be harvested and planted during the dormant season, preferably in March. Poles should be installed at 10-foot spacing using an auger or waterjet to create a hole for planting to a minimum depth of 4 feet.

## 7 Opinion of Probable Construction Cost

An opinion of the probable construction costs was developed for the proposed project (Table 7-1). A detailed breakdown of materials, work, and related costs is included in Appendix G.

The opinion of probable construction costs incorporates the following:

- 10% allowance for mobilization/demobilization
- 8.0% sales tax rate

The total construction cost includes a 10% construction contingency to reflect uncertainty in the schedule for bidding and items that may change prior to or during construction. The design has been developed to the 90% design level. The costs in Table 7-1 only include an opinion of the probable construction cost that would be borne by the construction contractor. Engineering, permitting, and administration costs are not included in this opinion of probable cost. Most of the engineering, permitting, and administration work to be completed during the design phase has already been funded. Additional funding may be needed to administer and manage the project through construction.

Costs were divided into base bid items and the following optional bid items:

- Option A Bid Items Includes modification to the stream channel at the lower point of diversion, including reworking of boulders to eliminate drops in the channel upstream of RM 7.71. This work may not be required or desired as part of the final bid package.
- Option B Bid Items This includes installation of corrugated polyethylene pipe to replace the
  irrigation ditch east of U.S. Highway 97. KCCD may decide not to construct this segment of
  pipeline if there is not budget to support the work.
- Option C Bid Items This includes cottonwood copse planting. KCCD anticipates that this work
  may be completed by volunteers or others under a separate contract.

### 7.1.1 Assumptions

The following assumptions are reflected in the opinion of costs:

- The pipeline installed from the intake to Burke Road will be installed within an existing ditch easement. No additional easements or property acquisition will be required for this pipeline.
- The pipeline along Burke Road will be installed entirely within Kittitas County right-of-way and will be subject to a franchise agreement being developed between the ranch owner and the County. Any costs associated with that franchise agreement are assumed to be the responsibility of the ranch owner and are not included.
- WDFW will furnish and oversee installation of the rotating drum fish screen. The costs include contractor labor to transport the screen to the site from the Yakima Screen Shop, remove the

- existing fish screen, excavate to accommodate the new fish screen, prepare subgrade, place and compact foundation material, and assist WDFW with screen installation.
- The contractor will also trench, place and compact backfill, and install the fish bypass pipeline and connect that pipeline to the modular fish screen.
- One-third of streambed boulders will be sourced on site.
- No export of streambed materials will be required.

The opinion of probable construction cost will be refined through the detailed design.

Table 7-1
Opinion of Probable Construction Costs

ltem	Opinion of Probable Cost	
Base Bid Items:		
Division 1 – General Requirements	\$48,000	
Division 2 – Existing Conditions	\$18,000	
Division 31 – Earthwork	\$86,000	
Division 32 – Exterior Improvements	\$46,000	
Division 33 – Utilities	\$57,000	
Construction Subtotal - Base Bid Items	\$255,000	
Sales Tax (8.0%)	\$20,400	
Subtotal – Construction Contract – Base Bid Items	\$275,000	
Contingency (10%)	\$27,500	
Total Construction Cost – Base Bid Items	\$303,000	
Option A Bid Items (Channel Restoration at RM 7.71):		
Division 31 – Earthwork	\$5,000	
Division 32 – Exterior Improvements	\$8,000	
Construction Subtotal – Option A Bid Items	\$13,000	
Sales Tax (8.0%)	\$1,040	
Subtotal – Construction Contract – Option A Bid Items	\$14,000	
Contingency (10%)	\$1,400	
Total Construction Cost – Option A Bid Items	\$15,000	
Option B Bid Items (Irrigation Pipeline East of Highway 97)		
Division 31 – Earthwork	\$21,000	
Division 33 – Utilities	\$31,000	
Construction Subtotal – Option B Bid Items	\$52,000	
Sales Tax (8.0%)	\$4,160	
Subtotal – Construction Contract – Option B Bid Items	\$56,000	
Contingency (10%)	\$5,600	
Total Construction Cost - Option B Bid Items	\$62,000	

Item	Opinion of Probable Cost	
Option C Bid Items (Cottonwood Copse Planting):		
Division 32 – Exterior Improvements	\$11,000	
Construction Subtotal – Option C Bid Items	\$11,000	
Sales Tax (8.0%)	\$880	
Subtotal – Construction Contract – Option C Bid Items	\$12,000	
Contingency (10%)	\$1,200	
Total Construction Cost – Option C Bid Items	\$13,000	
Total – Base Bid and All Optional Bid Items:		
Construction Subtotal	\$331,000	
Sales Tax (8.0%)	\$26,480	
Subtotal – Construction Contract	\$357,000	
Contingency (10%)	\$35,700	
Total Construction Cost	\$393,000	

#### Notes:

- 1. Intake facilities include preparing the screen structure for screen installation.
- 2. Pipeline costs include trenching; furnishing and installing pipe, fittings, and appurtenances; backfilling; compaction of backfill; surface repair; and hanging pipeline on bridge.
- 3. Subtotals and totals are rounded up to the nearest \$1,000.
- 4. Costs are in 2020 dollars.

### 8 Summary and Recommendations

This report summarizes the design of The Ranch on Swauk Creek Diversion Improvement and Restoration Project. The project will convert a portion of the existing open, unlined delivery ditch to a buried pipeline, upgrade the fish screen and bypass at the existing intake facility, and construct a roughened stream channel downstream from existing intake. The project will also remove a second, downstream intake structure and restore the channel in that location. Downstream of the irrigation infrastructure improvements, approximately 3.5 acres of riparian habitat will be planted with cottonwood poles to supplement prior riparian plantings. These improvements are intended to achieve the following objectives:

- Eliminate irrigation-related mortality of steelhead, coho, and Chinook salmon at Swauk Creek RM 7.71 and significantly reduce the irrigation-related mortality of steelhead, coho, and Chinook salmon at Swauk Creek RM 7.92.
- Restore year-round fish passage for all life stages of salmonids at Swauk Creek RM 7.71 and RM 7.92.
- Improve summer rearing conditions for juvenile steelhead, coho, and Chinook salmon in Swauk
   Creek by increasing irrigation efficiency, resulting in up to 0.25 cfs of conserved water available
   for instream flow benefits.
- Increase canopy cover, shade, and a source of future large woody debris for Swauk Creek and its floodplain by planting up to approximately 3.5 acres with cottonwood copses.

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# Appendix A Site Visit Notes and Photographs



## Meeting Minutes Kick-off Meeting/Site Visit

The Ranch on Swuak Creek Project 1:00 PM; April 29, 2020; Project Site

#### **Attendees**

David Rice, P.E. Anchor QEA

Merri Martz Anchor QEA

Ryan Roberts, P.E. Kittitas County Conservation District

Cassandra Weekes Washington Department of Fish and Wildlife

#### **Meeting Minutes/Site Visit Notes**

#### **WDFW Screen and Coordination**

- Josh from WDFW's screen shop was not able to attend the site visit.
- Dave will contact Josh and/or Danny at WDFW's screen shop and schedule some time to talk through screening options over the phone.
- The existing screen at the upstream diversion seems to do a decent job of keeping fish out of the
  irrigation canal, but it backwaters and does not offer consistent sweeping velocity to move fish
  past the screen and through the bypass back to the creek. The bypass sometimes appears to flow
  backwards towards the screen.
- At the time of the site visit, the water level in the creek appeared to be higher than the invert of
  the bypass at the screen, but there did not appear to be water backing up into the screen
  through the bypass, which would suggest that the bypass was plugged or has some kind of
  check feature.
- They are considering different options but there are two modular rotating drum screens available in the shop. If one of these screens looks like it is the correct size, this may be a good option.
- The ranch owner maintains the screen and the rest of the diversion system. The existing screen requires very frequent cleaning during the irrigation season (e.g. every 2 hours).

#### Kittitas County Conservation District (KCCD) Restoration Goals, Extents

• Streambed boulders were placed in channel at the upstream diversion in an effort to establish appropriate hydraulic head conditions when the screen was replaced about 10 years ago.

- The streambed boulders have either shifted or settled and are not maintaining the appropriate
  hydraulic conditions to keep water in the diversion during the late summer and to keep water
  moving past the screen with sweeping velocity.
- The ranch owner currently installs an aluminum pole across the stream channel with a plastic tarp
  draped over it and anchored to the stream bed to check up the water in the late summer to
  maintain diversions at the upstream diversion.
- The ranch owner currently installs cattle fencing with a plastic tarp draped over it and some temporary pipe extending up the left bank of the creek to capture enough water for the downstream diversion during the late summer low-flow period.
- The downstream diversion is not screened and entrains fish into the system.
- The ranch owner has to put the materials in the creek early in the season (sometimes as early as the first half of July) to get water.
- Both diversions are barriers to fish passage.
- KCCD and the ranch owner would like to see a fish-passable rock weir that maintains the
  appropriate hydraulic conditions to keep water in the diversion during the late summer low-flow
  period and maintains appropriate depth and sweeping velocity conditions at the new screen.
- Additional restoration work could include planting up to 1 acre of cottonwood copses in the riparian area downstream of Burke Road, where some previous restoration work occurred, but there are breaks in the riparian coverage.

#### **Irrigation Operations**

- The ranch uses the water as follows:
  - The upstream diversion conveys water to a canal that extends south, crossing Highway 97 and Burke Road, and delivers up to approximately 2 cfs to pasture that is south of Burke Road and west of Swauk Creek. The small ditch that extends east along Burke Road to Swauk Creek from the main canal spills excess water back to Swauk Creek.
  - The downstream diversion conveys water through pipes and open canal to a pond on the ranch property south of Burke Road and east of Swauk Creek. The ranch then irrigates pasture on the east side of Swauk Creek from the pond.
  - The total combined peak flow rate for the two diversions is 3.5 cfs. The upstream diversion has two water rights that each allow for diversion of up to 2 cfs, but the water rights are rotating, so the maximum diversion rate at any time is 2 cfs. The downstream diversion has a water right that allows for diversion of up to 1.5 cfs.

#### Franchise Agreement, Coordination with County Public Works

- The ranch owner has indicated that they are negotiating to obtain a franchise agreement with the County for domestic water and it would be ideal if the agreement also included irrigation water.
- Ryan indicated that it is not clear yet whether the franchise agreement exists and whether it will allow for burial of irrigation pipe along the edge of Burke Road.
- The proposed crossing at Swauk Creek would consist of hanging the pipe on the County's bridge where Burke Road crosses Swauk Creek. Ryan is not sure yet whether the County will allow this.
- If the pipe cannot be hung from the bridge, the downstream diversion may need to be supplied by a pipe crossing under Swauk Creek near the location of the diversion to send water through the upstream diversion into the existing lower pipe/canal system.
- Any property owner coordination would go through Ryan at KCCD.

#### Schedule, Timeline for Implementation

- If possible, they would like to start construction this fall when the irrigation season ends to avoid having another irrigation season with fish mortality and fish barriers.
- That would require permitting on a very short timeline (would need permits in hand by September).
- Cassandra will verify the in-water work window (verified after the meeting as July 15 to September 30). An extension into October is likely to be feasible.
- They will use BPA as the federal lead for permitting, but with the Covid-19 situation, there have been some delays in Section 106 consultations.
- If needed, maybe we can consider doing the out-of-channel work in the spring before the irrigation season starts.
- Typically, they would like to submit permits with a 60% complete design to ensure that things do
  not change significantly as the permits are reviewed, but in this case the 30% design (with
  sufficient details) would likely need to be used for permitting.

#### **Action Items**

- Anchor QEA
  - Call Josh and Danny to discuss screen configurations and pin down the screen type and approach for installing it.
  - Look at the CAD survey file to verify the limitations on the data near Burke Road. Send request for additional survey data to Ryan.

o Review background information to verify what we have received and what we have not received. Request additional information, if needed.

#### Ryan

- o Coordinate with the ranch owner and the County Public Works Department to clarify the status of the franchise agreement between the County and the ranch owner, confirm whether the agreement will include irrigation water infrastructure, and determine whether pipe can be hung from the Burke Road Bridge over Swauk Creek.
- o Coordinate and contract with HLA to collect additional survey data, if needed.
- o Provide any other background information requested by Anchor QEA, if available.

#### Cassandra

- o Verify in-water work window. DONE, EMAILED TO ANCHOR QEA ON 4/30.
- Clarify level of design needed to initiate permitting. DONE. EMAILED TO ANCHOR QEA ON 4/30.
- Send WSDOT Report with additional flow information for upstream fish passage project.
   DONE. EMAIL TO ANCHOR QEA ON 4/30.

## **Site Photographs**



Photograph 1 - Diversion Structure with Slide Gate at Creek



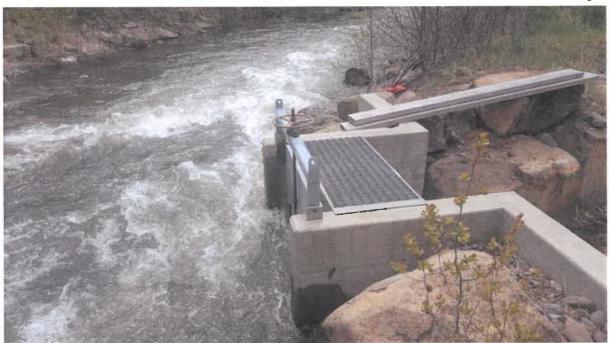
Photograph 2 – Fish Screen and Irrigation Canal from Diversion Structure



Photograph 3 – Fish Screen with Paddle Wheel



Photograph 4 – Channel at Diversion with Streambed Boulders



Photograph 5 – Diversion Structure and Channel Looking Downstream



Photograph 6 – Irrigation Canal Downstream of Fish Screen on West Side of Creek



Photograph 7 – Downstream Irrigation Diversion Structure



Photograph 8 – Culvert Inlet on Irrigation Canal on West Side of Creek at Highway 97



Photograph 9 – Upstream end of Culvert on West Side of Creek at Burke Road



Photograph 10 – Flow Control Structure on East Canal/Pipeline N Side of Burke Road



Photograph 11 – Pond at Downstream End of Canal on East Side of Swauk Creek



Photograph 12 – S Side of Burke Road Bridge Over Swauk Creek

# Appendix B Design Drawings

#### 90% DESIGN SUBMITTAL

## RANCH ON SWAUK CREEK IRRIGATION DIVERSION IMPROVEMENT AND RESTORATION

KITTITAS COUNTY CONSERVATION DISTRICT





SHEET #	DRAWING #	TITLE
-1	G01	COVER SHEET
2	G02	GENERAL NOTES, ABBREVIATIONS, AND LEGENDS
3	G03	SPA HIP III GENERAL CONSERVATION & IMPLEMENTATION MEASURES
4	G04	BPA HIP III GENERAL CONSERVATION & IMPLEMENTATION MEASURES
5	G05	OVERALL SITE PLAN
6	G05	SURVEY CONTROL PLAN
7	701	TEMPORARY ACCESS AND STAGING PLAN
8	102	TEMPORARY EROSION, SEDIMENT, AND WATER CONTROL PLAN
9	703	TESC NOTES
10	104	YESC DETAILS
11	C01	DIVERSION IMPROVEMENT AND RESTORATION PLAN (RM 7.92)
12	C02	DIVERSION IMPROVEMENT AND RESTORATION PLAN (RM 7.71)
13	C03	STREAM CHANNEL PROFILES
14	004	STREAM CHANNEL SECTIONS
15	* 005	RESTORATION AND FISH BYPASS DETAILS
16	C06	RESTORATION PLANTING PLAN AND DETAILS
17	CII	IRRIGATION PIPELINE PLAN AND PROFILE (STA 0+00 TO STA 11+20)
18	C12	(RRIGATION PIPELINE PLAN AND PROFILE (STA 11+20 TO STA 22+80)
19	C13	(RRIGATION PIPELINE PLAN AND PROFILE (STA 22+80 TO END)
20	C14	IRRIGATION PIPELINE TYPICAL SECTIONS AND DETAILS
21	CIS	IRRIGATION PIPELINE DETAILS
22	C16	(RRIGATION PIPELINE DETAILS

THE RANCH AT SWAUK CREEK KITTITAS CO. PARCELS B27336, 195535, 949

ONTRACTING AGENCY:

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SCREENING/PERMITTING: CASSANDRA WEEKS WASHINGTON DEPT. OF

ENGINEER: DAVID R ANCHOL

DAVID RICE, P.E. ANCHOR QEA, LLC 720 OLIVE WAY, SUITE 1900 SEATTLE, WA 98101 (206) 219-5902

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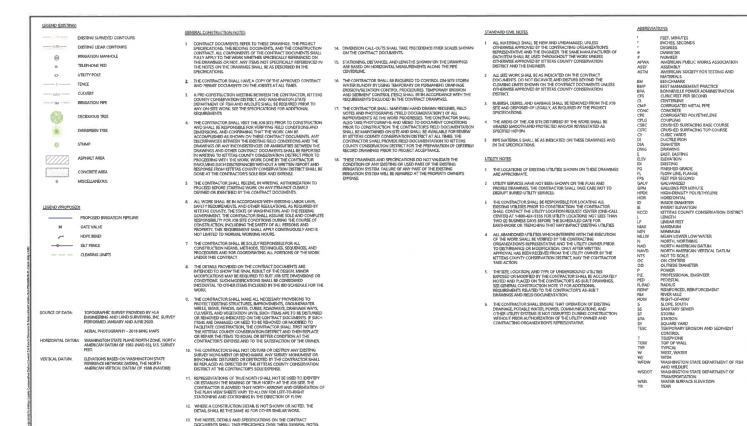


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  - B. EQUIPMENT ENTRY AND EXIT POINTS:
  - ROAD AND STREAM CROSSING ALIGNMENTS.
  - D. STAGING, STORAGE, AND STOCKPILE AREAS; AND
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- V. SEDIMENT WILL BE REMOVED FROM BROSION CONTROLS ONCE IT HAS REACHED 1/3 OF THE EXPOSED HEIGHT OF THE CONTROL.
- VI. ONCE THE SITE IS STABILIZED AFTER CONSTRUCTION, TEMPORARY EROSION CONTROL MEASURES WILL BE REMOVED.
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CONSTRUCTION AND POST-CONSTRUCTION CONSERVATION MEASURES.

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  TREATMENTS TO REMAYED BEINE AND OTHER POLICIAN OF PROSERVE WILL
  REPROVIDED.

RANCH ON SWAUK CREEK

ANCHOR QEA

KITTITAS COUNTY CONSERVATION DISTRICT REV DATE BY APP'D

SCALE AS MOTED

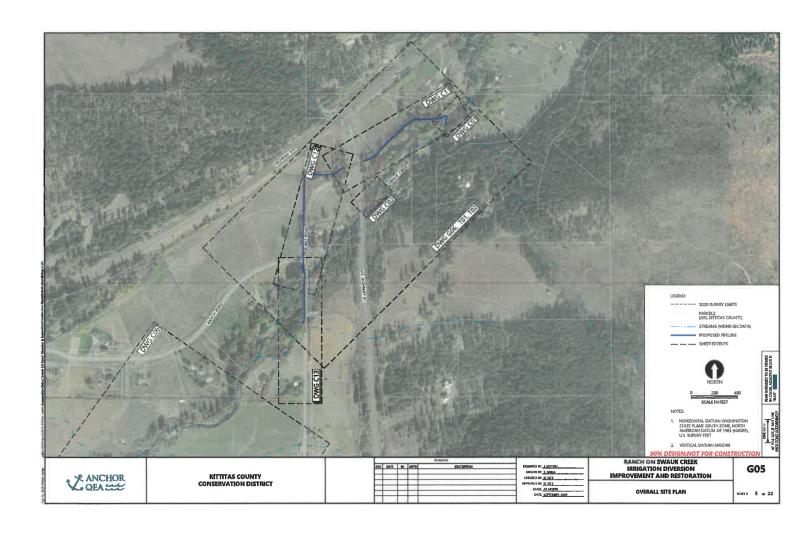
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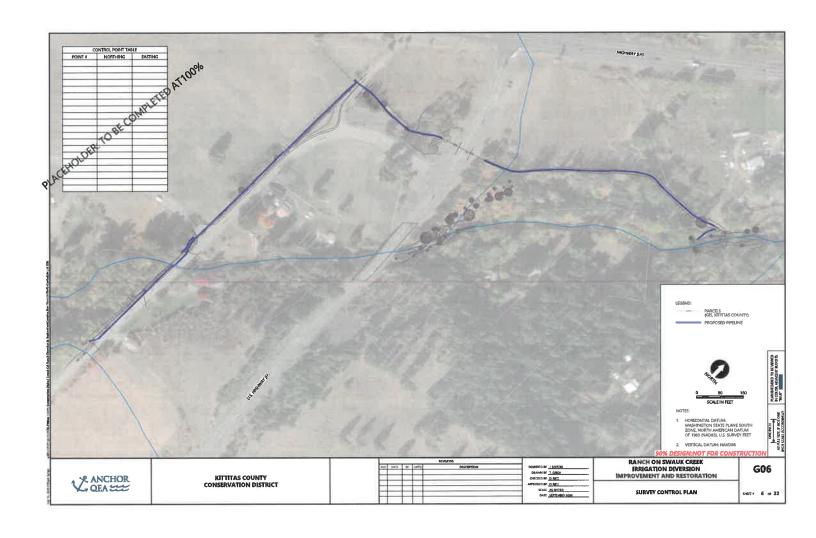
IRRIGATION DIVERSION IMPROVEMENT AND RESTORATION BPA HIP III GENERAL CONSERVATION & IMPLEMENTATION MEASURES

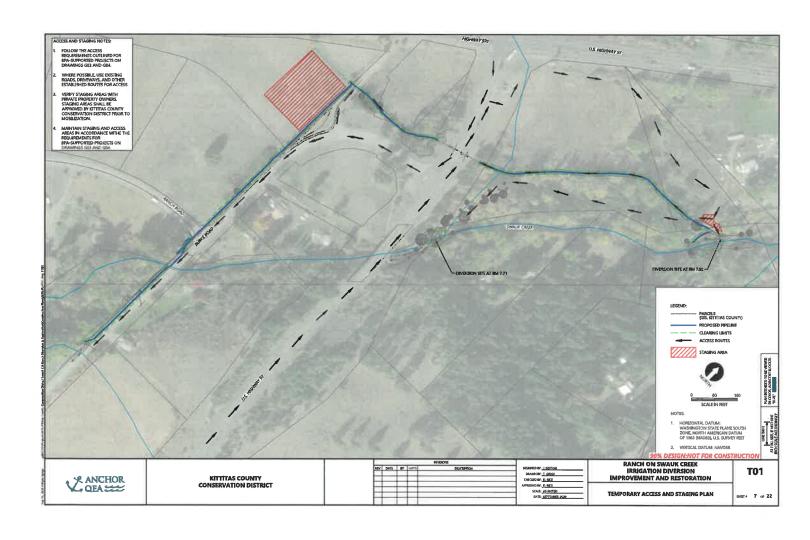
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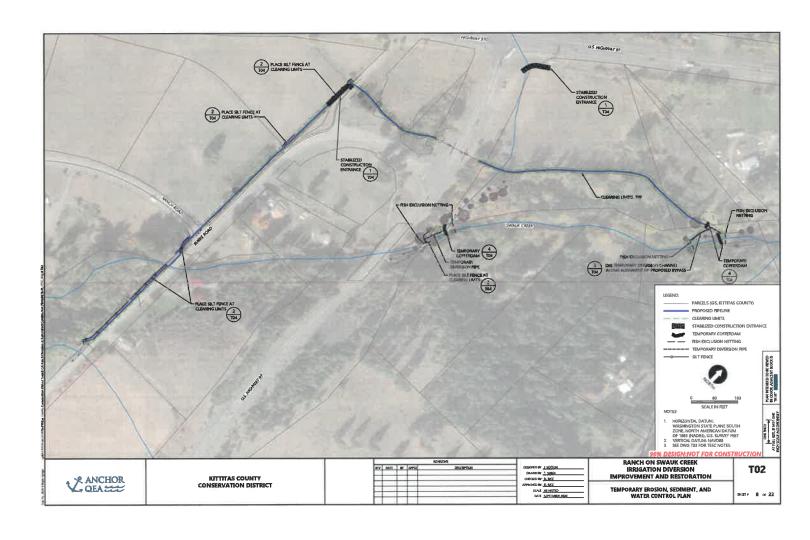
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**G04** 









GENERAL TEMPORARY ENDSIGN AND SEDWENT CONTROL (TISO NOTE):

- THE CONTRACTOR SHALL PROVIDE A CERTIFIED BROSIGN AND SEDIMENT CONTROL LEAD (CESCL) TO MANAGE AND MAINTAIN TEMPORARY EROSION AND SEDIMENT CONTROL FOR THE PROJECT. THE NAMED PRESON OR RIFM SHALL BE ON-STEE OR ON-CALL AT ALL TIMES.
- THE CLEARING LIMIT BOUNDARIES SHALL BE CLEARLY FLAGED IN THE FIELD PRIOR TO CONSTRUCTION. DUTING THE CONSTRUCTION PERIOD NO DISTURBANCE BEYOND THE FLAGED CLEARING LIMITS SHALL BE PRIMITTED. THE FLAGGING SHALL BE MAINTAINED BY THE CONTRACTOR FOR THE DURATION OF CONSTRUCTION.

- THE TEST FACILITIES SHALL BEINSPECTED DAILY BY THE CONTRACTOR-AND MAINTAINED, REPAIRED, OR AUGMENTED AS NECESSARY, TO ENSURE THEIR CONTINUED FUNCTIONING.
- CHARLES AND THE PROJECT.

  FORM OF CORREST THE PROJECT AND SERVICE SHALL SHARLD DEFORD AND LINVENESS.

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  AND LINVENESS DEFORM AND EXCESSED AND SERVICE SHALL SHARLD AND THE BUT AND SHAPE SHA
- SOIL AND OTHER STOCKPILES MUST BE STABILIZED AND PROTECTED WITH SEDIMENT-TRAPPING MEASURES.
- ALL POLLUTANTS, INCLUDING WASTE MATERIALS AND DEMOLITION DEBRIS, THAT OCCUR ON SITE DURING CONSTRUCTION SHALL BE HANDLED AND DISPOSED OF IN A MANNER THAT DOES NOT CAUSE CONTAMINATION OF STORMAYTER.

- 14. THE CONTRACTOR SHALL PRESERVE NATURAL LANDSCAPE, AND PRESERVE AND PROTECT BISSING VEGETATION NOT REQUIRED OR OTHERWISE AUTHORIZED TO BE REMOVED, AS OUTLINED IN THE SPECIFICATIONS.
- 15. REPAIR OR TREAT INJURED TREES AND VEGETATION AS REQUIRED BY THE SPECIFICATIONS.
- 16. REMOVE AND DISPOSE OF TIKES AND VEGETATION THAT ARE INJURED OR DAMAGED BEYOND SAMING AND NOT REQUIRED OR OTHERWISE AUTHORIZED FOR REMOVAL AS REQUIRED IN THE SPECIFICATIONS. REPLACE THE INJURIED TIKE OR SHRUB AS DIRECTED BY ECCODE REPRESENTATIVE.

#### PROJECT SPECIFIC TESC NOTES

- THE TESC PLAN DRAWINGS SHOWN ARE CONCEPTUAL. THE CONTRACTOR IS REQUIRED TO SUBMI DETAILED TESC PLANS AND A CONSTRUCTION STORMWATER POLLUTION PREVENTION PLAN SWIPPS TO RCCD'S REPRESENTATIVE FOR APPROVAL PER THE REQUIREMENTS OF THE CONTRACT DOCUMENTS.
- THE CONTRACTOR IS RESPONSIBLE FOR THE CARE AND DIVERSION OF WATER DURING CONSTRUCTION IN ACCORDANCE WITH LOCAL STATE, AND FEDERAL WATER QUALITY STANDARD
- THE CONTRACTOR SHALL BYSURE NECESSARY PRECAUTIONS SHALL BE TAKEN TO PREVENT ANY CEMENT CONCRETE OR BYPRODUCTS, ASPHALT CONCRETE OR BYPRODUCTS, OR ANY DISCHARGE FROM SAM CUTTING AND FLANING FROM BEING DISCHARGED INTO ANY STORM DRAIN OR SUFFACE WATER SYSTEM.
- TESC IMPLÉMENTATION AND MAINTÉNANCE SHALL COMPLY WITH ALL PROJECT PÉRMIT RECOLURRIGENTS.
- THE CONTRACTOR SHALL NOT FUEL EQUIPMENT OR STORE FUEL AT ELEVATIONS LOWER THAN 5 FEET ABOVE THE ORDINARY HIGH WATER (OHW) OF THE NEAREST STREAM OR SURFACE WATER RETURN
- WASHING OF EQUIPMENT ON THE PROJECT SITE SHALL NOT BE ALLOWED UNLESS AUTHORIZED IN WRITING BY KCCD'S REPRESENTATIVE.

#### CONSTRUCTION SEQUENCE

- FLAG CLEARING LIMITS AND EXISTING TREES TO REMAIN.
- 3. CONSTRUCT STABILIZED CONSTRUCTION ENTRANCES.
- INSTALL SILT PENCE
- COMPLETE CLEARING AND REMOVAL OF EXISTING STRUCTURES AND OBSTRUCTIONS ABOVE THE OHMM, INCLUDING THE DISTING RISH SCREEN AND OTHER IRRIGATION EQUIPMENT TO BE REPLACED.
- Britall Temporary Water Diversion Facilities and Dewater the Portion of the Edisting Stream Channel to Be Modified.
- COMPLETE IN-CHANNEL WORK, INCLUDING MOVING AND PLACING IN-CHANNEL ROCK AND OTHER MATERIALS.
- 8. REMOVE TEMPORARY WATER DIVERSION FACILITIES ONCE IN-CHANNEL WORK IS COMPLETE
- 9. EXCAVATE FOR FISH SCREENING AND BYPASS FACILITIES.
- 10. INSTALL FISH SCREENING AND BYPASS FACILITIES.
- 11. EXCAVATE AND TRENCH FOR INSTALLATION OF IRRIGATION DELIVERY PIPELINE.
- BACKFILL TRENCHES AND EXCAVATIONS AS SOON AS POSSIBLE AFTER INSTALLATION OF BURIED PIPE AND APPLICATIONALIS.
- 14. COMPLETE SURFACE REPAIR AND PLANTING
- DURING CONSTRUCTION, MAINTAIN AND UPGRADE TESC BMPS AS NEEDED TO PREVENT SEDIMENT FROM LEAVING THE SITE.
- 16. REMOVE TESC BMPS AFTER SURFACE IS REPAIRED AND/OR SEEDED AND GROWING

SEQUENCE SHALL BE ADAPTED, AS NEEDED, FOR OPTIONAL TEMS INCLUDED DURING CONSTRUCTION.

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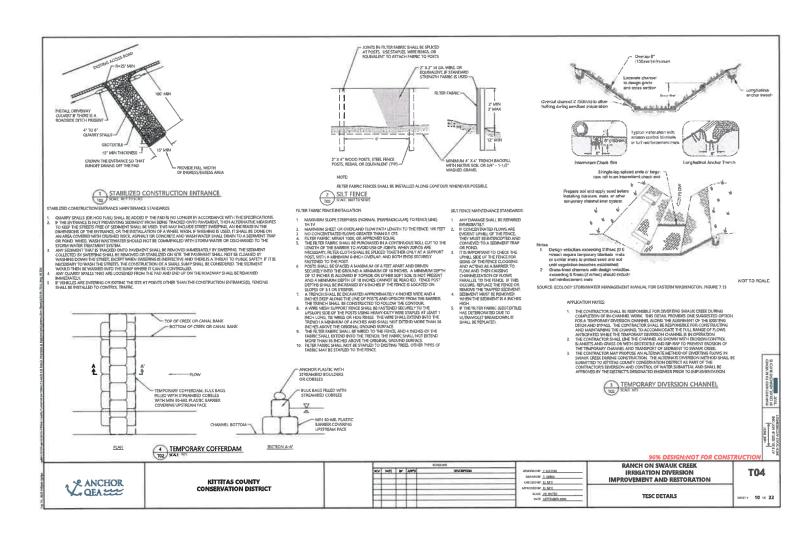
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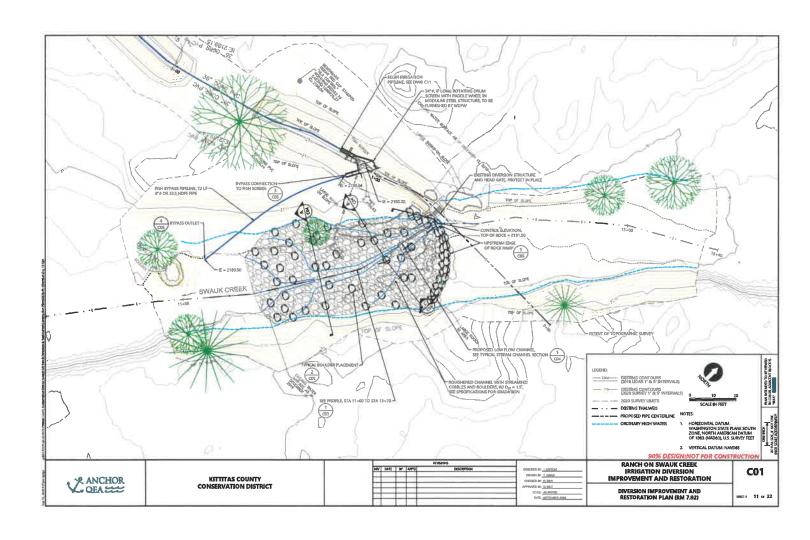
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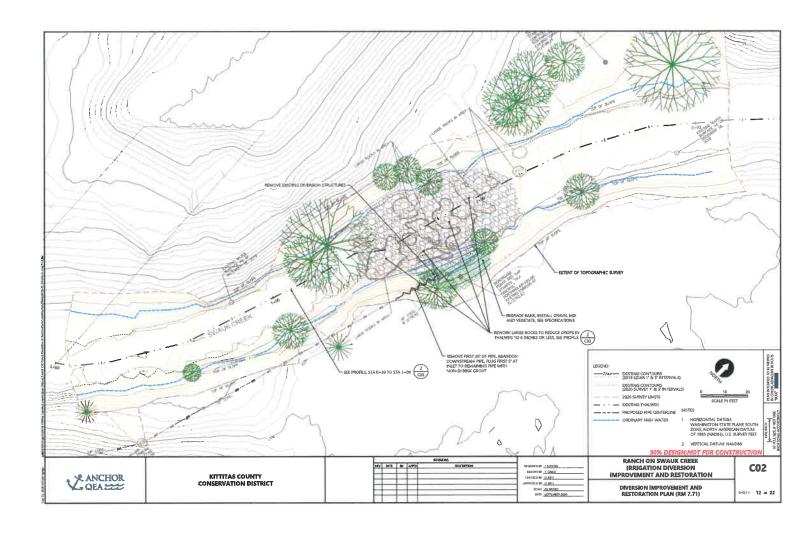
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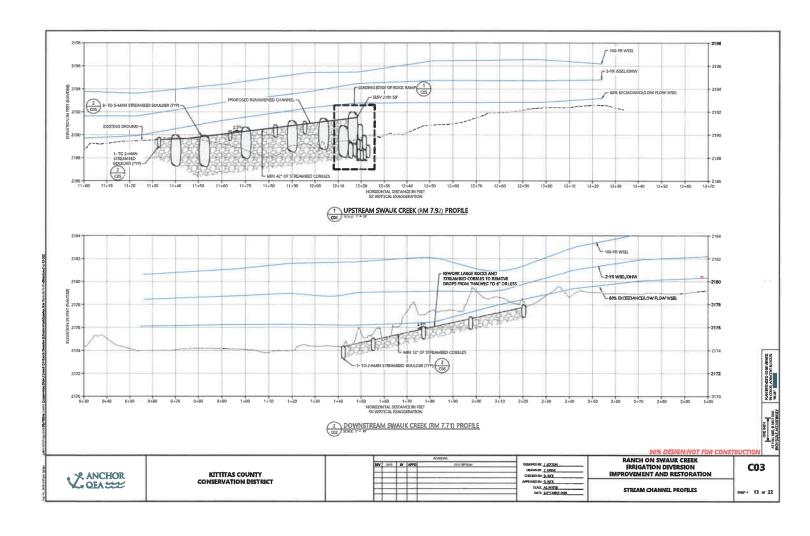
RANCH ON SWAUK CREEK **IRRIGATION DIVERSION** IMPROVEMENT AND RESTORATION TESC NOTES

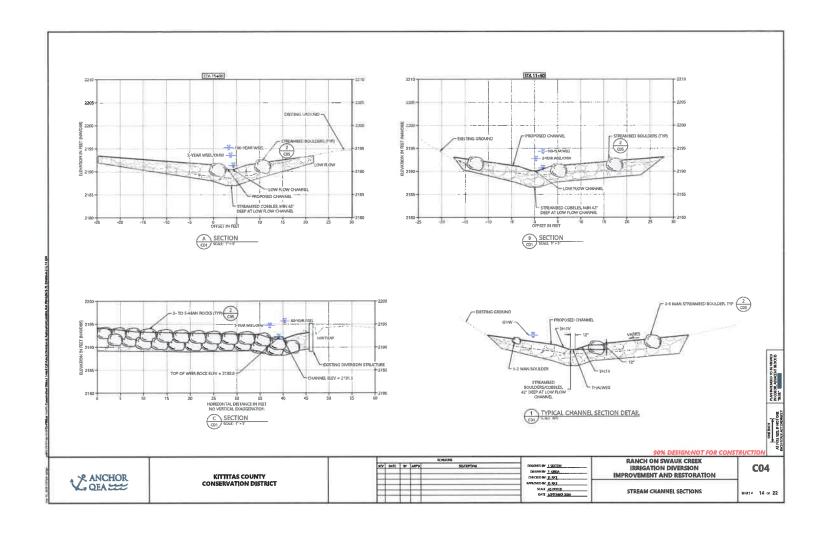
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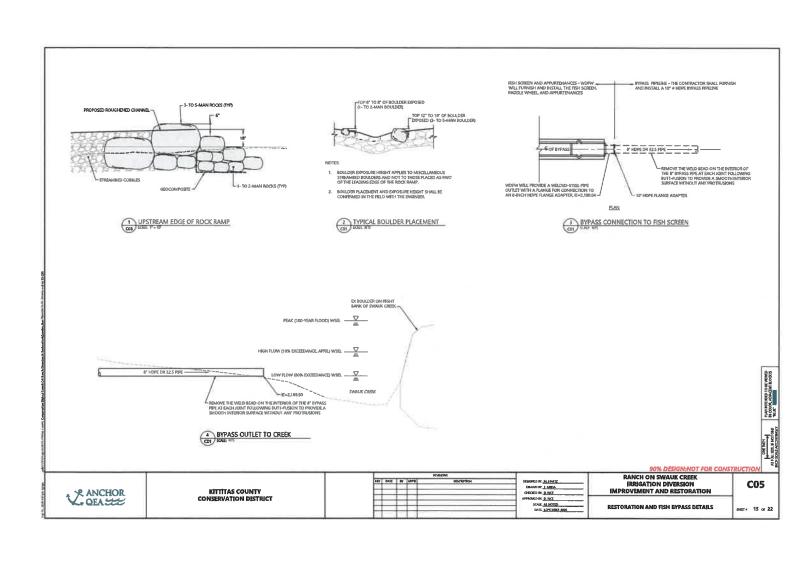


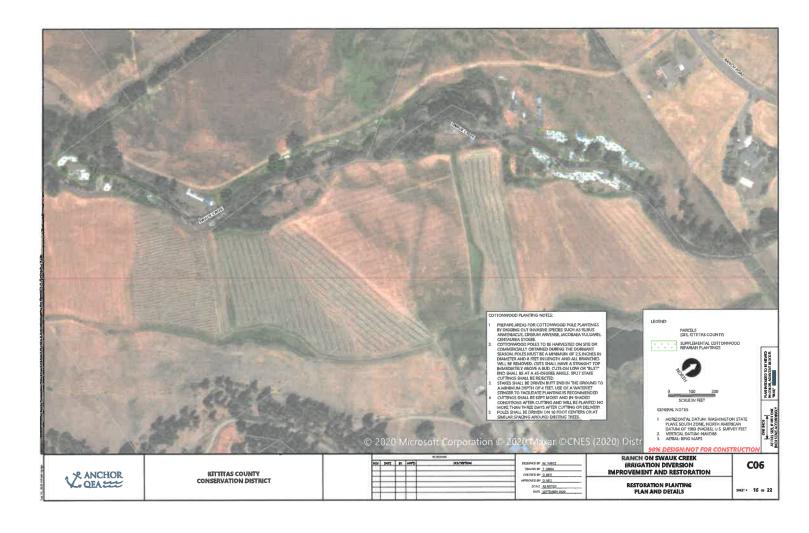


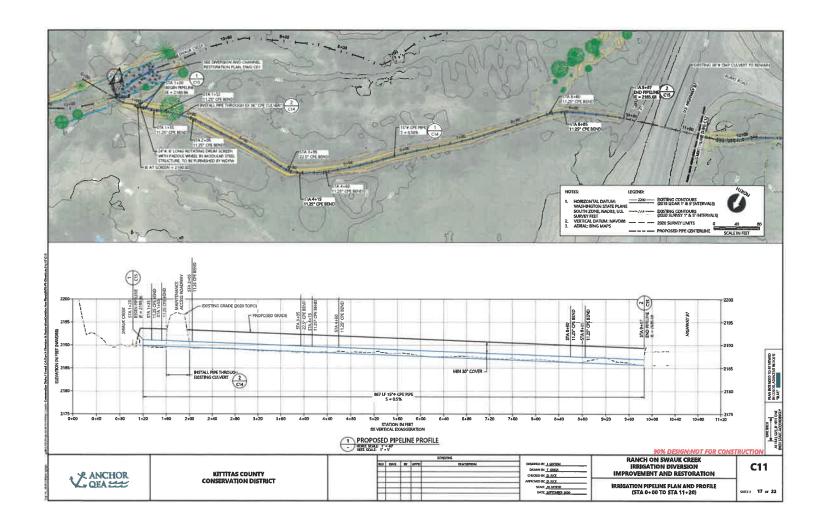


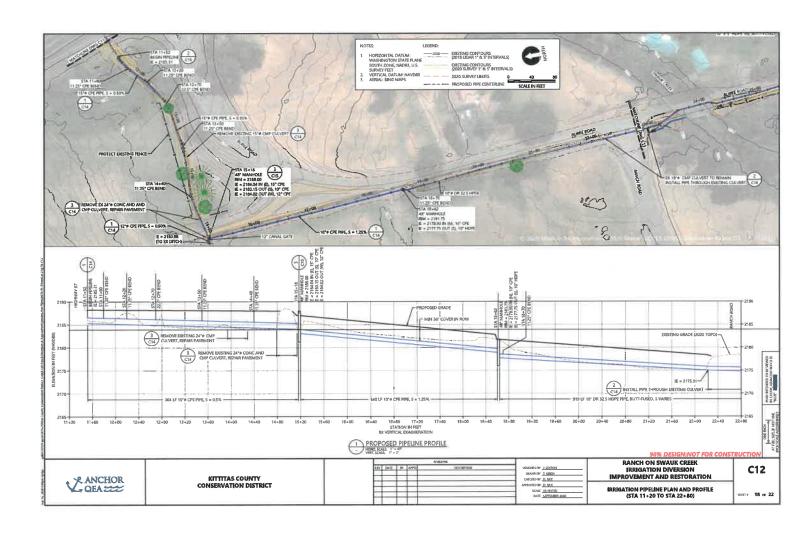


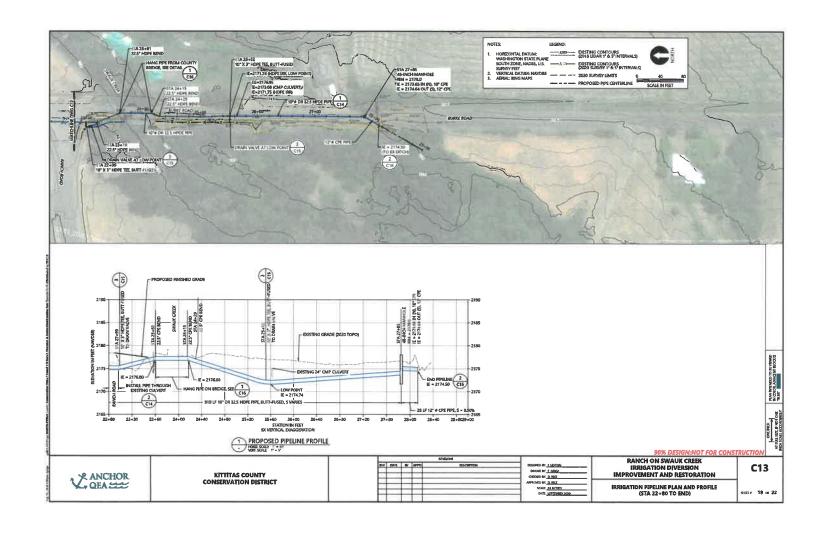


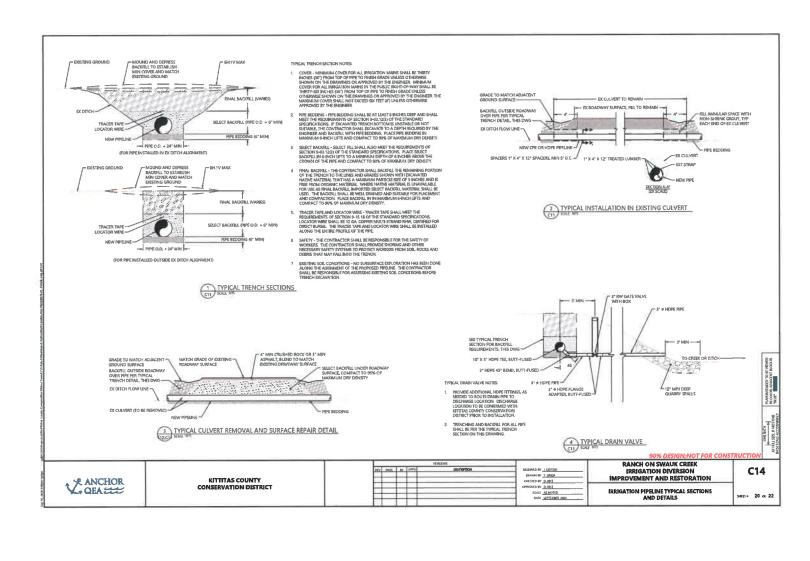


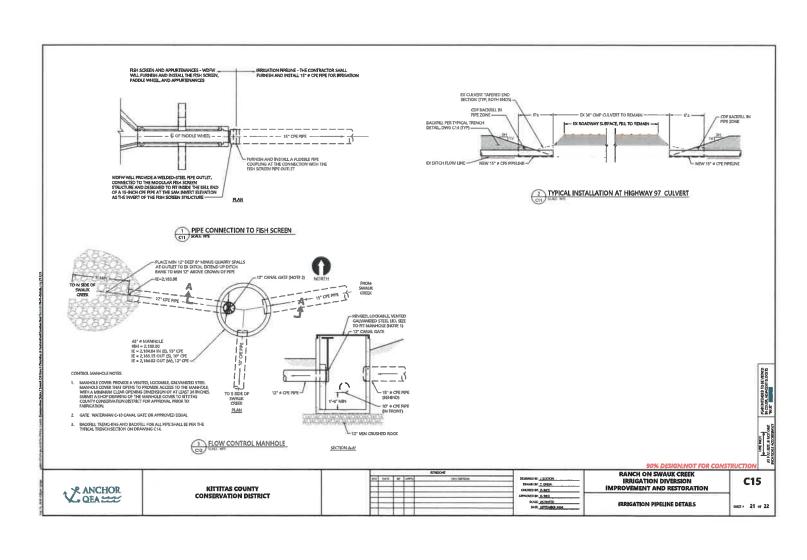


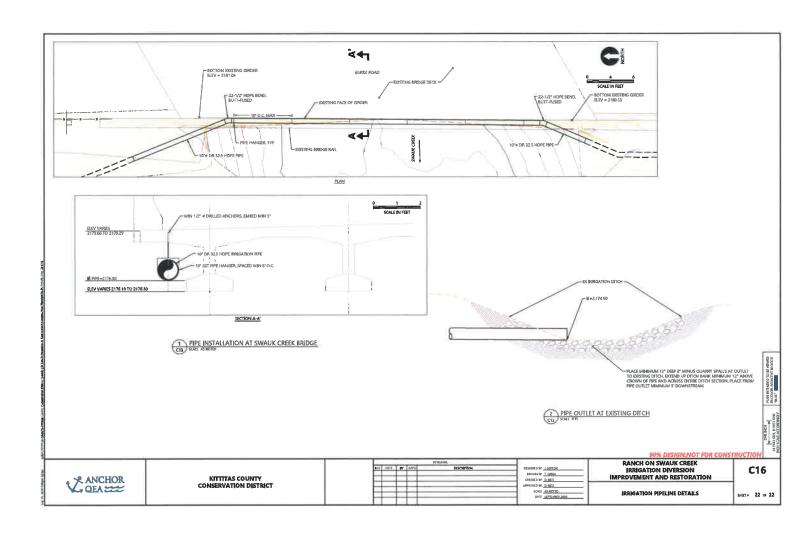












# Appendix C Trust Water Right Analysis

The Ranch on Swauk Creek (The Ranch) currently has rights to divert up to 3.5 CFS of flow from Swauk Creek between two diversions at RM 7.92 and 7.71. The current SRFB application for The Ranch proposes to consolidate these diversion to the upper location. A detailed trust water analysis at this location had previously not been defined which left some questions as to the possibility of dewatering the creek between the diversions. After researching the water rights that affect diversion quantities at the upper location, the likelihood of dewatering the creek between the diversions appears to be very low. Justification for this conclusion is summarized below.

#### Summary of trust water rights at Swauk Creek RM 7.92 and in the upper watershed

Historic irrigation diversions from within the Swauk Creek watershed consist of one diversion from First Creek, a left bank tributary to Swauk Creek at approximately RM 8.4 and two diversions from Swauk Creek, which are the target of the current SRFB application. The First Creek diversion is located at approximately RM 3.9. The water rights within the Swauk watershed have priority dates ranging from Nov 2, 1877 to Oct 31 1889. The First Creek water rights are all from the 1877 date and have seniority over all others. The water rights for the diversion at Swauk RM 7.92 & 7.71 are from 1878 junior only to First Creek rights. Due to that fact, only water rights from 1877 and 1878 have an effect on trust water passing the subject diversion and will be the only rights addressed in this summary.

Table 1 describes the water rights from 1877 and 1878. Appendix A provides greater detail for the individual rights that make up each of the three columns in Table 1.

<b>Priority Date</b>	1877		1878	1878		
Owner	Suncadia/Roan	Th	ne Ranch	Suncadia		
Purpose	Instream/Mitigation	Irrigation		Irrigation		Instream
Creek	First		Swauk	Swauk		
April	3.23	3.50	91.15%	0.34		
May	3.45	3.50	89.97%	0.39		
June	3.51	3.50	89.74%	0.40		
July	3.61	3.50	89.29%	0.42		
August	3.55	3.50	89.74%	0.40		
September	3.39	3.50	90.44%	0.37		
October	3.04	3.50	91.86%	0.31		

Table 1

Trust quantities are shown in cubic feet per second (CFS) and vary based upon the month of the irrigation season. The 1877 trust water is composed of water from four different trust applications from two owners and the 1878 trust and irrigation water is composed of water from five different applications and two owners.

#### First Creek Trust Quantity

The amount of First Creek trust water is established at the point of diversion at RM 3.9 and is expected to remaining within the system well below the Swauk Creek diversion at RM 7.92. The amount of trust water may be adjusted if the flow within First Creek, as measured at the mouth, is below the trust quantity in Table 1. At that point, the measured quantity is expected to pass the Swauk RM 7.92 diversion. Swauk Creek Trust Quantity

Due to identical priority dates and diversion locations for the irrigation and trust water from 1878, the water within Swauk Creek is prorated to each use. The percentage of water diverted to The Ranch for irrigation purposes is shown in Table 1.

#### **Trust Calculation Scenarios**

Due to flow variation within First and Swauk Creeks, the amount of trust water can be significantly affected as low flows occur during the mid to later summer months. Below are potential flow scenarios, but do not represent all possible combination of creek flows between First and Swauk Creeks. These scenarios represent the most likely outcomes during periods of low flow.

- 1. Flow within First and Swauk Creeks are at or above the combined water quantities for trust water and irrigation. Under this scenario, the full quantity of First Creek trust water and full quantity of Swauk Creek trust water is expected to pass the Swauk RM 7.92 diversion. The full quantity of irrigation water may be diverted from Swauk Creek.
- 2. Flow within First Creek is below the quantities listed in Table 1 while flow within Swauk Creek remains at or above the combined 1878 quantities from Table 1 after subtracting First Creek flows. Under this scenario, the trust water from First Creek is reduced to the flow quantity measured at the mouth. This quantity plus the full Swauk trust quantity is expected to pass the RM 7.92 diversion. The full quantity of irrigation rights can be diverted, but only provided by Swauk Creek flows.
- 3. Flows within both First and Swauk Creeks are below the trust quantities and combined irrigation and trust quantities, respectively, provided in Table 1. Under this scenario, the trust water from First Creek is again reduced to the flow quantity measured at the mouth. The flow within Swauk Creek is reduced by the quantity measured at First Creek and then prorated based upon the percentages in Table 1. The full flow from First Creek is now considered trust water and expected to pass RM 7.92 diversion while the Swauk trust water will be prorated per Table 1. The quantity of irrigation water diverted is based on the prorated factor applied to Swauk Creek flows only.

Minor changes in Swauk Creek flows may occur between the mouth of First Creek and the Swauk RM 7.92 diversion, but are assumed to insignificant in the above scenarios.

#### In-stream flows based on historical flow data

Starting in 2014, the DOE has been tracking flows at the mouth of First Creek and in Swauk Creek immediately downstream of the confluence via remote gaging stations. Based upon those numbers and applying the appropriate scenario described above, Table 2 shows how much trust water would have been expected to pass the Swauk Creek RM 7.92 diversion.

Water (CFS) Passing Diversions Based on Trust Water & DOE Flow Stations											
Month / Year	2014	2015	2016	2017	2018	2019					
April		28.8	200.3	243.3	194.3	131.3					
May	No Data	12.9	78.6	162.0	165.0	58.6					
June		4.6	12.8	36.6	19.5	9.9					
July	4.7	2.03	3.8	6.2	2.8	4.3					
August	1.9	1.5	- hara	1.3	0.92	1.77					
Sept	1.52	1.68	No Data	0.96	1.01	1.69					
Oct	1.7	2.9		5.7	2.01	No Data					

Table 2

The DOE stations and data can be found at the following web addresses.

Mouth of First Creek

https://fortress.wa.gov/ecy/eap/flows/station.asp?sta=39S050

Swauk Creek below First Creek

https://fortress.wa.gov/ecy/eap/flows/station.asp?sta=39M130

If the proposed project is successfully implemented, including all piping, there is a possibility of increasing existing trust water passing the Swauk RM 7.92 diversion by 0.25 CFS. Swauk Creek between RM 7.92 and the confluence with the Yakima River may be flow limited based upon levels of yearly precipitation. Additional trust water would improve the potential for minimizing those periods during low water years.

### Appendix A

Claimant Name	New Suncadia LLC	J.P. Roan	New Suncadia LLC	J.P. Roan
Claim #	00648	00648	00648	0648
Certificate #	S4-84770-J	S4-85121-J	S4-85193-J	S4-85197-J
Source	First Creek	First Creek	First Creek	First Creek
Use	Instream flow & mitigation	Instream flow & mitigation	Instream flow & mitigation	Instream flows
Period of Use	April 1 thru Oct 15	April 1 thru Oct 15	April 1 thru Oct 15	April 1 thru Oct 15
Month	1 44 5 15 4 1 PER 1 4 1 F			
April	1.18	0.11	0.55	1.394
May	1.33	0.11	0.62	1.394
June	1.37	0.11	0.64	1.394
July	1.44	0.11	0.67	1.394
August	1.40	0.11	0.65	1.394
September	1.29	0.11	0.60	1.394
October	1.03	0.11	0.51	1.394
Priority Date	Nov 2, 1877	Nov 2, 1877	Nov 2, 1877	Nev 2, 1877
POD	First Creek RM 3.9	First Creek RM 3.9	First Creek RM 3.9	First Creek RM 3.9

Claimant Name	The Ranch on Swauk	The Ranch on Swauk	The Ranch on Swauk	New Suncadia LLC	New Suncadia LLC
Claim #	01475	01475	01475	01685	01685
Certificate #	S4-83887-J	S4-83890-J	\$4-84343-J	S4-83893-J	S4-85211-J
Source	Swauk Crk & Two Wells	Swauk Creek	Swauk Creek	Swauk Creek	Swauk Creek
Use	Irrigation 18.37 ac	Irrigation 78.4 ac & Stockwater	Irrigation 19.8 ac & Stockwater	Instream flows	Instream flows
Period of Use	April 1 thru Oct 31	April 1 thru Oct 31	April 1 thru Oct 31	April 1 thru Oct 15	April 1 thru Oct 15
Month					
April	1.50	2.00	1.50	0.23	0.11
May	1.50	2.00	1.50	0.26	0.13
June	1.50	2.00	1.50	0.27	0.13
July	1.50	2.00	1.50	0.28	0.14
August	1.50	2.00	1.50	0.27	0.13
September	1.50	2.00	1.50	0.25	0.12
October	1.50	2.00	1.50	0.21	0.10
Priority Date	June 30, 1878	June 30, 1878	June 30, 1878	June 30, 1878	June 30, 1878
POD	NW1/4, NW1/4, Sec 27	Lower Diversion	Upper Diversion	Upper Diversion	Upper Diversion

# Appendix D Swauk Creek Hydraulic Analysis

## Kittitas Conservation District The Ranch at Swauk Creek Diversion Improvement and Restoration Project

**Existing Conditions** 

Existing Co	-									
River Sta	Q Total	Manning n	Min Ch El	Max Chl Dpth	W.S. Elev	Vel Chnl	Shear Chan	Flow Area	Top Width	Froude # Chl
	(cfs)		(ft)	(ft)	(ft)	(ft/s)	(lb/sq ft)	(sq ft)	(ft)	
7165.97	1180	0.045	2218.25	4.24	2222.49	4.65	0.84	309.51	172.07	0.45
7165.97	498	0.045	2218.25	3.27	2221.52	4.98	1.08	102.07	114.39	0.58
7165.97	356	0.045	2218.25	2.88	2221.13	4.32	0.86	82.86	93.22	0.55
7165.97	264	0.045	2218.25	2.59	2220.84	3.77	0.69	70.05	84.01	0.52
7165.97	4.6	0.045	2218.25	0.62	2218.87	0.81	0.06	5.71	19.95	0.27
7165.97	3.5	0.045	2218.25	0.57	2218.82	0.74	0.05	4.74	18.38	0.26
6877.12	1180	0.045	2216.21	3.45	2219.66	8.09				
6877.12	498	0.045	2216.21	2.22	2218.43					
6877.12	356	0.045	2216.21	1.87	2218.08	5.16	1.35	68.93		
6877.12	264	0.045	2216.21	1.58	2217.79	4.76	1.22	55.51	46.1	0.76
6877.12	4.6	0.045	2216.21	0.19	2216.4	1.87	0.42	2.46	22.61	1
6877.12	3.5	0.045	2216.21	0.17	2216.38	1.75	0.39	2	21.69	1.02
6650.42	1180	0.045	2213.29	3.75	2217.04	7.35	2.12			
6650.42	498	0.045	2213.29	2.6	2215.89	5.11	1.19	98.14		
6650.42	356	0.045	2213.29	2.24	2215.54	4.44	0.95	80.26	47.63	
6650.42	264	0.045	2213.29	1.94	2215.23	3.99	0.8	66.14		
6650.42	4.6	0.045	2213.29	0.28	2213.57	0.76	0.06	6.07		
6650.42	3.5	0.045	2213.29	0.25	2213.54	0.67	0.05	5.23	30.32	0.28
6424.86	1180	0.045	2210.75	4.91	2215.66	5.88	1.25	227.01	84.8	0.52
6424.86	498	0.045	2210.75	3.21	2213.96	5.09	1.13	99.4	48.42	0.59
6424.86	356	0.045	2210.75	2.73	2213.48	4.6	0.99	77.62	44.08	0.6
6424.86	264	0.045	2210.75	2.35	2213.11	4.29	0.92	61.56	40.49	0.61
6424.86	4.6	0.045	2210.75	0.24	2210.99	2.14	0.51	2.15	15.42	1.01
6424.86	3.5	0.045	2210.75	0.21	2210.96	2.09	0.51	1.68	14.68	1.09

1

6259.81	1180	0.045	2209.7	4.25	2213.95	8.17	2.43	152.2	46.27	0.73
6259.81	498	0.045	2209.7	3.35	2213.05	4.6	0.84	112.07	42.49	0.47
6259.81	356	0.045	2209.7	2.95	2212.65	3.82	0.61	95.61	40.83	0.41
6259.81	264	0.045	2209.7	2.65	2212.35	3.23	0.45	83.47	39.5	0.37
6259.81	4.6	0.045	2209.7	0.51	2210.21	0.48	0.02	9.53	28.83	0.15
6259.81	3.5	0.045	2209.7	0.46	2210.16	0.43	0.02	8.23	28.57	0.14
6079.35	1180	0.045	2209.43	2.6	2212.03	6.25	1.82	216.54	193.59	0.81
6079.35	498	0.045	2209.43	1.72	2211.15	5.68	1.85	87.72	88.79	1
6079.35	356	0.045	2209.43	1.52	2210.95	5.1	1.61	69.83	87.36	1.01
6079.35	264	0.045	2209.43	1.34	2210.77	4.87	1.55	54.16	79.56	1.04
6079.35	4.6	0.045	2209.43	0.21	2209.64	1.62	0.33	2.84	30.53	0.94
6079.35	3.5	0.045	2209.43	0.19	2209.62	1.52	0.31	2.3	30.23	0.97
5902.35	1180	0.045	2205.98	3.43	2209.41	5.44	1.2	255.12	146.15	0.57
5902.35	498	0.045	2205.98	2.54	2208.52	4.08	0.76	138.5	112.14	0.51
5902.35	356	0.045	2205.98	2.22	2208.2	3.72	0.67	105.12	97.05	0.51
5902.35	264	0.045	2205.98	2.01	2207.99	3.25	0.54	86.19	84.64	0.48
5902.35	4.6	0.045	2205.98	0.5	2206.48	0.66	0.04	7	30.87	0.24
5902.35	3.5	0.045	2205.98	0.48	2206.46	0.53	0.03	6.55	30.25	0.2
5773.55	1180	0.045	2205.46	2.06	2207.52	6.94	2.37	170.95	112.61	0.97
5773.55	498	0.045	2205.46	1.39	2206.85	5.12	1.55	97.24	106.61	0.95
5773.55	356	0.045	2205.46	1.28	2206.74	4.14	1.05	86.01	105.38	0.81
5773.55	264	0.045	2205.46	1.13	2206.59	3.75	0.92	70.43	103.72	0.8
5773.55	4.6	0.045	2205.46	0.3	2205.76	0.95	0.11	4.86	41.45	0.49
5773.55	3.5	0.045	2205.46	0.21	2205.67	1.82	0.4	1.92	18.74	1
5598.93	1180	0.045	2201.13	3.48	2204.61	6.69	1.9	176.9	73.13	0.75
5598.93	498	0.045	2201.13	2.23	2203.36	5.25	1.39	94.84	63.35	0.76
5598.93	356	0.045	2201.13	1.84	2202.97	5.09	1.44	69.89	62.67	0.85
5598.93	264	0.045	2201.13	1.64	2202.77	4.57	1.22	57.74	60.86	0.83
5598.93	4.6	0.045	2201.13	0.21	2201.34	1.93	0.43	2.38	18.93	0.96
5598.93	3.5	0.045	2201.13	0.28	2201.41	0.95	0.09	3.69	21.1	0.4

5245.6	1180	0.045	2194.98	4.69	2199.67	8.84	2.89	148.91	93.05	0.79
5245.6	498	0.045	2194.98	3.08	2198.06	6.63	1.91	75.16	31.82	0.76
5245.6	356	0.045	2194.98	2.74	2197.72	5.53	1.38	64.39	30.51	0.67
5245.6	264	0.045	2194.98	2.27	2197.25	5.2	1.29	50.74	28.12	0.68
5245.6	4.6	0.045	2194.98	0.21	2195.19	2.05	0.49	2.24	18.44	1.04
5245.6	3.5	0.045	2194.98	0.2	2195.18	1.77	0.38	1.98	18.37	0.95
5069.13	1180	0.045	2192.22	4	2196.22	11.36	4.94	133.46	83.86	1.06
5069.13	498	0.045	2192.22	3.17	2195.39	7.6	2.41	75.01	53.39	0.81
5069.13	356	0.045	2192.22	2.58	2194.8	7.4	2.48	50.25	33.61	0.89
5069.13	264	0.045	2192.22	2.31	2194.53	6.36	1.91	41.92	28.44	0.81
5069.13	4.6	0.045	2192.22	0.61	2192.83	0.62	0.03	7.39	18.01	0.17
5069.13	3.5	0.045	2192.22	0.58	2192.8	0.52	0.02	6.73	17.8	0.15
5043.89	1180	0.045	2192.55	3.29	2195.84	9.73	3.85	132.19	61.51	1
5043.89	498	0.045	2192.55	1.92	2194.47	8.64	3.65	58.34	42.66	1.18
5043.89	356	0.045	2192.55	1.75	2194.3	6.91	2.4	51.51	33.54	0.98
5043.89	264	0.045	2192.55	1.51	2194.06	6.03	1.92	43.78	33.05	0.92
5043.89	4.6	0.045	2192.55	0.2	2192.75	1.13	0.13	4.08	25.7	0.5
5043.89	3.5	0.045	2192.55	0.17	2192.72	1.01	0.11	3.46	25.6	0.48
4997.51	1180	0.045	2191.29	3.59	2194.88	9.61	3.63	128.38	50.49	0.95
4997.51	498	0.045	2191.29	2.14	2193.43	7.57	2.74	66.42	38.48	1
4997.51	356	0.045	2191.29	1.78	2193.07	6.8	2.37	52.72	37.77	1
4997.51	264	0.045	2191.29	1.53	2192.82	6.17	2.08	43.05	37.25	1
4997.51	4.6	0.045	2191.29	0.26	2191.55	2.26	0.55	2.03	12.89	1.01
4997.51	3.5	0.045	2191.29	0.23	2191.52	2.11	0.5	1.66	12.24	1.01
4965.06	1180	0.045	2189.59	5.08	2194.67	8.11	2.25	164.36	52.08	0.65
4965.06	498	0.045	2189.59	3.53	2193.12	5.84	1.33	95.25	40.02	0.57
4965.06	356	0.045	2189.59	3.05	2192.64	5.21	1.11	76.5	37.55	0.55
4965.06	264	0.045	2189.59	2.67	2192.26	4.74	0.97	62.71	36.05	0.54
4965.06	4.6	0.045	2189.59	0.65	2190.24	0.78	0.05	5.87	14.21	0.21

4965.06	3.5	0.045	2189.59	0.61	2190.2	0.66	0.03	5.3	14.11	0.19
4943.6	1180	0.045	2189.7	5.06	2194.76	6.16	1.37	207.15	59.68	0.53
4943.6	498	0.045	2189.7	3.29	2192.99	5.26	1.14	95.43	36.69	0.56
4943.6	356	0.045	2189.7	2.83	2192.53	4.51	0.88	79.08	34.32	0.52
4943.6	264	0.045	2189.7	2.47	2192.17	3.93	0.7	67.11	32.47	0.48
4943.6	4.6	0.045	2189.7	0.54	2190.24	0.37	0.01	12.49	24.39	0.09
4943.6	3.5	0.045	2189.7	0.5	2190.2	0.3	0.01	11.56	24.23	0.08
4908.09	1180	0.045	2189.59	4.75	2194.34	6.65	1.74	177.35	55.77	0.66
4908.09	498	0.045	2189.59	3.12	2192.71	5.21	1.21	95.55	44.41	0.63
4908.09	356	0.045	2189.59	2.62	2192.21	4.8	1.09	74.1	40.79	0.63
4908.09	264	0.045	2189.59	2.24	2191.83	4.46	0.99	59.16	37.94	0.63
4908.09	4.6	0.045	2189.59	0.61	2190.2	0.81	0.07	5.66	29.14	0.33
4908.09	3.5	0.045	2189.59	0.58	2190.17	0.74	0.06	4.76	28.94	0.32
4871.2	1180	0.045	2189.43	4.75	2194.18	6.27	1.39	203.57	61.02	0.53
4871.2	498	0.045	2189.43	3.1	2192.53	4.6	0.88	112.87	48.89	0.49
4871.2	356	0.045	2189.43	2.57	2192	4.18	0.78	87.88	45.1	0.5
4871.2	264	0.045	2189.43	2.16	2191.59	3.86	0.7	70.03	42.37	0.5
4871.2	4.6	0.045	2189.43	0.22	2189.65	2.06	0.49	2.23	17.95	1.03
4871.2	3.5	0.045	2189.43	0.2	2189.63	1.87	0.42	1.87	16.55	0.98
4847.25	1180	0.045	2189.05	5.25	2194.3	4.12	0.64	286.22	79.19	0.38
4847.25	498	0.045	2189.05	3.52	2192.57	3.04	0.39	163.75	62.8	0.33
4847.25	356	0.045	2189.05	2.97	2192.02	2.73	0.33	130.51	58.03	0.32
4847.25	264	0.045	2189.05	2.54	2191.59	2.47	0.28	106.8	54.49	0.31
4847.25	4.6	0.045	2189.05	0.5	2189.55	0.36	0.01	12.85	37.3	0.11
4847.25	3.5	0.045	2189.05	0.46	2189.51	0.31	0.01	11.43	36.98	0.1
4775.33	1180	0.045	2189.21	3.97	2193.09	8.26	2.66	154.82	71.29	0.79
4775.33	498	0.045	2189.21	2.64	2191.76	6.04	1.64	82.44	37.69	0.72
4775.33	356	0.045	2189.21	2.2	2191.33	5.34	1.35	66.61	35.05	0.68
4775.33	264	0.045	2189.21	1.86	2190.98	4.81	1.15	54.83	33.78	0.67

4775.33	4.6	0.045	2189.21	0.3	2189.42	1.24	0.18	3.7	30.86	0.63
4775.33	3.5	0.045	2189.21	0.28	2189.4	1.1	0.15	3.17	30.8	0.61
4646.06	1180	0.045	2187.16	3.71	2190.87	7.6	2.73	155.37	85.48	0.99
4646.06	498	0.045	2187.16	2	2189.16	7.42	2.67	67.14	39.19	1
4646.06	356	0.045	2187.16	1.65	2188.81	6.66	2.3	53.49	38.79	1
4646.06	264	0.045	2187.16	1.43	2188.59	5.86	1.88	45.09	38.54	0.95
4646.06	4.6	0.045	2187.16	0.32	2187.48	1.03	0.11	4.47	26.31	0.44
4646.06	3.5	0.045	2187.16	0.29	2187.45	0.94	0.1	3.71	25.57	0.44
4540.24	1180	0.045	2185.06	4.13	2189.19	6.83	1.86	172.88	57.67	0.69
4540.24	498	0.045	2185.06	2.58	2187.64	5.41	1.32	92	44.27	0.66
4540.24	356	0.045	2185.06	2.14	2187.2	4.85	1.12	73.43	41.3	0.64
4540.24	264	0.045	2185.06	1.67	2186.73	4.84	1.2	54.59	38.81	0.72
4540.24	4.6	0.045	2185.06	0.16	2185.22	1.83	0.41	2.51	24.21	1
4540.24	3.5	0.045	2185.06	0.14	2185.2	1.6	0.33	2.18	23.88	0.94
4447.62	1180	0.045	2183.23	4.94	2188.17	7.08	1.99	166.76	53.12	0.7
4447.62	498	0.045	2183.23	3.26	2186.49	5.78	1.54	86.12	43.31	0.72
4447.62	356	0.045	2183.23	2.78	2186.02	5.38	1.41	66.19	38.94	0.73
4447.62	264	0.045	2183.23	2.25	2185.48	5.25	1.3	50.31	26.97	0.68
4447.62	4.6	0.045	2183.23	0.4	2183.63	0.86	0.07	5.33	21.43	0.31
4447.62	3.5	0.045	2183.23	0.36	2183.59	0.77	0.06	4.56	21.32	0.29
4321.17	1180	0.045	2182.22	5.02	2187.24	6.29	1.48	187.56	49.1	0.57
4321.17	498	0.045	2182.22	3.18	2185.4	4.86	1.03	102.45	43.16	0.56
4321.17	356	0.045	2182.22	2.61	2184.83	4.51	0.93	78.95	38.95	0.56
4321.17	264	0.045	2182.22	2.16	2184.38	4.25	0.86	62.14	34.19	0.56
4321.17	4.6	0.045	2182.22	0.25	2182.47	1.34	0.21	3.43	28.62	0.68
4321.17	3.5	0.045	2182.22	0.23	2182.45	1.23	0.19	2.84	28.21	0.68
4177.43	1180	0.045	2180.64	4.76	2185.4	8.31	2.72	141.93	43.36	0.81
4177.43	498	0.045	2180.64	3.13	2183.77	6.32	1.76	78.86	34.03	0.73
4177.43	356	0.045	2180.64	2.66	2183.3	5.6	1.43	63.58	30.68	0.69

4177.43	264	0.045	2180.64	2.29	2182.93	5.01	1.19	52.69	28.46	0.65
4177.43	4.6	0.045	2180.64	0.35	2180.99	0.9	0.08	5.1	22.19	0.33
4177.43	3.5	0.045	2180.64	0.32	2180.96	0.8	0.06	4.36	22.12	0.32
4050.15	1180	0.045	2179.81	4.75	2184.56	6.52	1.54	188.73	59.16	0.57
4050.15	498	0.045	2179.81	2.9	2182.71	5.04	1.09	99.22	42.31	0.57
4050.15	356	0.045	2179.81	2.38	2182.19	4.57	0.96	77.97	39.75	0.57
4050.15	264	0.045	2179.81	2.01	2181.82	4.16	0.84	63.53	37.7	0.56
4050.15	4.6	0.045	2179.81	0.21	2180.02	1.02	0.11	4.52	29.48	0.46
4050.15	3.5	0.045	2179.81	0.18	2179.99	0.92	0.1	3.79	29.39	0.45
4019.45	1180	0.045	2179.46	4.8	2184.26	6.87	1.74	172.93	47.09	0.61
4019.45	498	0.045	2179.46	2.98	2182.44	5.25	1.19	94.83	38.61	0.59
4019.45	356	0.045	2179.46	2.46	2181.92	4.73	1.03	75.27	37	0.58
4019.45	264	0.045	2179.46	2.08	2181.54	4.28	0.89	61.66	36.09	0.58
4019.45	4.6	0.045	2179.46	0.28	2179.74	0.92	0.08	5	26.92	0.38
4019.45	3.5	0.045	2179.46	0.25	2179.71	0.84	0.07	4.19	26.51	0.37
3989.98	1180	0.045	2179.22	3.79	2183.01	10.06	3.94	119.27	40.27	0.97
3989.98	498	0.045	2179.22	2.22	2181.44	7.93	2.94	62.79	32.62	1.01
3989.98	356	0.045	2179.22	1.86	2181.08	6.96	2.39	51.14	31.51	0.96
3989.98	264	0.045	2179.22	1.57	2180.79	6.25	2.03	42.25	30.56	0.94
3989.98	4.6	0.045	2179.22	0.19	2179.41	1.27	0.17	3.63	24.31	0.58
3989.98	3.5	0.045	2179.22	0.17	2179.39	1.1	0.14	3.18	24.21	0.53
3957.3	1180	0.045	2178.47	3.2	2181.67	11.46	5.43	103.71	39.34	1.21
3957.3	498	0.045	2178.47	2.09	2180.56	7.95	3.03	62.65	34.97	1.05
3957.3	356	0.045	2178.47	1.77	2180.24	6.92	2.43	51.43	34.49	1
3957.3	264	0.045	2178.47	1.55	2180.02	6	1.92	44.02	34.18	0.93
3957.3	4.6	0.045	2178.47	0.3	2178.77	1.37	0.2	3.37	21.29	0.6
3957.3	3.5	0.045	2178.47	0.26	2178.73	1.32	0.2	2.66	20.56	0.65
3929.03	1180	0.045	2177.38	4.8	2182.19	6.62	1.61	191.8	63.74	0.58
3929.03	498	0.045	2177.38	2.4	2179.78	7.68	2.92	64.84	40.12	1.07

3929.03	356	0.045	2177.38	2.1	2179.48	6.71	2.35	53.06	38.9	1.01
3929.03	264	0.045	2177.38	1.85	2179.23	6.11	2.08	43.18	38.55	1.02
3929.03	4.6	0.045	2177.38	0.42	2177.8	2.54	0.65	1.81	9.8	1.04
3929.03	3.5	0.045	2177.38	0.39	2177.77	2.24	0.51	1.56	8.56	0.92
3894.78	1180	0.045	2175.66	5.86	2181.52	8.36	2.35	151.37	35.55	0.65
3894.78	498	0.045	2175.66	3.92	2179.58	5.94	1.39	87.22	30.84	0.59
3894.78	356	0.045	2175.66	3.34	2179	5.26	1.16	69.73	29.43	0.57
3894.78	264	0.045	2175.66	2.89	2178.55	4.77	1.02	56.58	28.32	0.57
3894.78	4.6	0.045	2175.66	0.31	2175.97	2.06	0.47	2.23	15.32	0.95
3894.78	3.5	0.045	2175.66	0.27	2175.93	1.99	0.47	1.75	15.23	1.04
3866.61	1180	0.045	2175.35	5.95	2181.3	8.28	2.29	149.86	33.28	0.63
3866.61	498	0.045	2175.35	4.1	2179.45	5.49	1.16	92.54	29.11	0.51
3866.61	356	0.045	2175.35	3.53	2178.88	4.71	0.91	76.36	27.67	0.48
3866.61	264	0.045	2175.35	3.08	2178.43	4.14	0.74	64.11	26.48	0.46
3866.61	4.6	0.045	2175.35	0.44	2175.8	0.74	0.04	6.25	18.31	0.22
3866.61	3.5	0.045	2175.35	0.4	2175.75	0.65	0.04	5.36	18.19	0.21
3843.82	1180	0.045	2175.35	5.74	2181.09	8.32	2.38	146.21	33.95	0.65
3843.82	498	0.045	2175.35	3.95	2179.3	5.52	1.21	90.28	28.26	0.54
3843.82	356	0.045	2175.35	3.4	2178.75	4.73	0.94	75.21	26.6	0.5
3843.82	264	0.045	2175.35	2.96	2178.31	4.13	0.74	63.89	25.23	0.46
3843.82	4.6	0.045	2175.35	0.41	2175.76	0.62	0.03	7.47	19.28	0.17
3843.82	3.5	0.045	2175.35	0.37	2175.72	0.53	0.02	6.6	19.18	0.16
3803.77	1180	0.045	2175.34	5.28	2180.62	8.75	2.67	141.38	36.15	0.71
3803.77	498	0.045	2175.34	3.61	2178.96	5.86	1.38	85.85	30.03	0.59
3803.77	356	0.045	2175.34	3.1	2178.44	5.05	1.09	70.87	28.52	0.56
3803.77	264	0.045	2175.34	2.69	2178.03	4.46	0.9	59.26	27.5	0.53
3803.77	4.6	0.045	2175.34	0.32	2175.66	0.93	0.08	4.92	20.17	0.33
3803.77	3.5	0.045	2175.34	0.28	2175.62	0.84	0.07	4.17	20.09	0.33
3763.5	1180	0.045	2175.12	5.53	2180.66	6.94	1.66	183.25	47.82	0.55

3763.5	498	0.045	2175.12	3.66	2178.78	5.16	1.06	101.77	39.25	0.51
3763.5	356	0.045	2175.12	3.11	2178.23	4.59	0.89	80.94	36.57	0.49
3763.5	264	0.045	2175.12	2.69	2177.81	4.12	0.75	65.94	34.36	0.47
3763.5	4.6	0.045	2175.12	0.35	2175.47	0.83	0.06	5.52	22.73	0.3
3763.5	3.5	0.045	2175.12	0.31	2175.43	0.75	0.05	4.69	22.68	0.29
3520.45	1180	0.045	2174	4.72	2178.72	7.76	2.15	159.93	51.16	0.66
3520.45	498	0.045	2174	3.17	2177.17	5.31	1.17	94.34	36.8	0.57
3520.45	356	0.045	2174	2.66	2176.66	4.68	0.97	76.09	34.77	0.55
3520.45	264	0.045	2174	2.27	2176.27	4.21	0.83	62.73	33.35	0.54
3520.45	4.6	0.045	2174	0.33	2174.33	0.85	0.07	5.41	25.29	0.32
3520.45	3.5	0.045	2174	0.3	2174.3	0.76	0.06	4.58	25.12	0.32
3328.42	1180	0.045	2172.65	4.47	2177.13	7.86	2.21	174.58	75.31	0.68
3328.42	498	0.045	2172.65	3.03	2175.68	5.66	1.32	90.28	38.25	0.6
3328.42	356	0.045	2172.65	2.55	2175.2	4.93	1.06	73.1	34.76	0.57
3328.42	264	0.045	2172.65	2.19	2174.84	4.36	0.88	60.89	33.11	0.55
3328.42	4.6	0.045	2172.65	0.23	2172.88	1.11	0.13	4.16	23.94	0.47
3328.42	3.5	0.045	2172.65	0.2	2172.85	1	0.11	3.49	23.76	0.46
3027.98	1180	0.045	2169.26	3.67	2172.93	9.72	3.66	127.86	46.27	0.95
3027.98	498	0.045	2169.26	2.3	2171.56	7.54	2.63	67.61	41	0.96
3027.98	356	0.045	2169.26	1.96	2171.22	6.63	2.17	54.17	38.46	0.93
3027.98	264	0.045	2169.26	1.69	2170.96	5.92	1.84	44.59	34.15	0.91
3027.98	4.6	0.045	2169.26	0.3	2169.56	1.18	0.13	3.9	18.91	0.46
3027.98	3.5	0.045	2169.26	0.26	2169.52	1.06	0.12	3.29	18.29	0.44
2983.9	1180	0.045	2168.33	3.29	2171.62	10.41	4.59	115.32	51.97	1.16
2983.9	498	0.045	2168.33	2.83	2171.16	5.44	1.34	92.04	48.23	0.67
2983.9	356	0.045	2168.33	2.46	2170.79	4.76	1.1	74.82	45.1	0.65
2983.9	264	0.045	2168.33	2.14	2170.47	4.32	0.95	61.04	42	0.63
2983.9	4.6	0.045	2168.33	0.26	2168.6	2.41	0.59	1.91	10.61	1
2983.9	3.5	0.045	2168.33	0.23	2168.56	2.29	0.55	1.53	9.52	1.01

2823.31	1180	0.045	2166.92	4.28	2171.2	5.41	1.12	261.93	140.81	0.52
2823.31	498	0.045	2166.92	3.23	2170.15	4.07	0.72	129.73	91.42	0.48
2823.31	356	0.045	2166.92	2.88	2169.8	3.52	0.57	103.11	62.57	0.45
2823.31	264	0.045	2166.92	2.57	2169.49	3.15	0.48	84.88	55.95	0.43
2823.31	4.6	0.045	2166.92	0.47	2167.39	0.72	0.05	6.43	24.04	0.24
2823.31	3.5	0.045	2166.92	0.43	2167.35	0.64	0.04	5.47	23.53	0.23
2472.76	1180	0.045	2164.51	2.91	2167.42	8.05	2.73	156.47	80.21	0.89
2472.76	498	0.045	2164.51	1.78	2166.29	6.55	2.19	76.75	57.91	0.97
2472.76	356	0.045	2164.51	1.47	2165.98	6.03	2.01	59.11	54.37	1.01
2472.76	264	0.045	2164.51	1.25	2165.77	5.51	1.77	47.91	49.93	0.99
2472.76	4.6	0.045	2164.51	0.18	2164.69	1.77	0.39	2.61	27.88	1.02
2472.76	3.5	0.045	2164.51	0.16	2164.67	1.68	0.38	2.08	27.1	1.07
2151.63	1180	0.045	2159.74	3.5	2163.24	5.21	1.1	242.45	148	0.55
2151.63	498	0.045	2159.74	2.3	2162.04	3.99	0.78	126.75	84.31	0.55
2151.63	356	0.045	2159.74	2.05	2161.79	3.38	0.59	106.14	81.36	0.51
2151.63	264	0.045	2159.74	1.83	2161.57	3.01	0.49	88.3	78.73	0.49
2151.63	4.6	0.045	2159.74	0.4	2160.14	0.88	0.07	5.24	22.85	0.32
2151.63	3.5	0.045	2159.74	0.34	2160.08	0.87	0.07	4	17.23	0.32
1781.43	1180	0.045	2155.44	3.06	2158.5	8.71	3.22	136.98	59.9	0.97
1781.43	498	0.045	2155.44	2.09	2157.53	6.02	1.78	82.79	52.11	0.84
1781.43	356	0.045	2155.44	1.65	2157.09	5.87	1.84	60.63	48.41	0.92
1781.43	264	0.045	2155.44	1.4	2156.84	5.39	1.64	48.94	46.3	0.93
1781.43	4.6	0.045	2155.44	0.23	2155.67	1.71	0.36	2.69	26.55	0.95
1781.43	3.5	0.045	2155.44	0.21	2155.65	1.63	0.34	2.15	23.76	0.96
1289.9	1180	0.045	2149.26	3.75	2153.01	6.54	1.63	183.09	56.93	0.62
1289.9	498	0.045	2149.26	2.26	2151.52	4.92	1.11	101.42	52.12	0.62
1289.9	356	0.045	2149.26	1.98	2151.24	4.08	0.8	87.32	51.1	0.55
1289.9	264	0.045	2149.26	1.7	2150.96	3.62	0.66	73.02	50.06	0.53
1289.9	4.6	0.045	2149.26	0.28	2149.54	0.69	0.05	6.64	43.14	0.31
1289.9	3.5	0.045	2149.26	0.26	2149.52	0.62	0.04	5.65	42.86	0.3

1002.97	1180	0.045	2145.6	3.24	2148.84	9.32	3.56	127.79	49.29	0.98
1002.97	498	0.045	2145.6	2.23	2147.83	6.19	1.81	80.51	44.6	0.81
1002.97	356	0.045	2145.6	1.69	2147.29	6.25	2.03	56.92	41.91	0.95
1002.97	264	0.045	2145.6	1.42	2147.02	5.74	1.82	45.96	40.59	0.95
1002.97	4.6	0.045	2145.6	0.2	2145.8	1.73	0.38	2.66	28.02	0.99
1002.97	3.5	0.045	2145.6	0.18	2145.78	1.6	0.34	2.19	27.17	1
719.85	1180	0.045	2142.91	3.66	2146.57	5.25	1.08	241.68	104.26	0.52
719.85	498	0.045	2142.91	2.38	2145.29	4.03	0.76	124.68	71.42	0.52
719.85	356	0.045	2142.91	2.23	2145.14	3.14	0.47	114.14	70.07	0.42
719.85	264	0.045	2142.91	1.97	2144.88	2.75	0.38	96.11	67.41	0.4
719.85	4.6	0.045	2142.91	0.29	2143.2	0.58	0.03	7.96	36.42	0.22
719.85	3.5	0.045	2142.91	0.25	2143.16	0.52	0.03	6.72	35.27	0.21
460	1180	0.045	2141.32	2.12	2143.44	7.55	2.68	159.61	135.2	0.99
460	498	0.045	2141.32	1.63	2142.95	4.44	1.03	112.98	89.89	0.68
460	356	0.045	2141.32	1.12	2142.44	5.12	1.6	69.53	83.67	0.99
460	264	0.045	2141.32	0.97	2142.29	4.66	1.4	56.71	81.06	0.98
460	4.6	0.045	2141.32	0.21	2141.53	1.43	0.27	3.23	38.56	0.87
460	3.5	0.045	2141.32	0.19	2141.51	1.33	0.24	2.64	35.58	0.86
135.22	1180	0.045	2134.32	2.99	2137.31	4.39	0.96	269.52	178.9	0.62
135.22	498	0.045	2134.32	2.56	2136.88	5.8	1.88	85.86	162.73	0.98
135.22	356	0.045	2134.32	2.69	2137.01	3.71	0.74	96.09	164.62	0.6
135.22	264	0.045	2134.32	2.48	2136.8	3.31	0.63	79.78	161.69	0.58
135.22	4.6	0.045	2134.32	0.96	2135.28	1.54	0.2	3	39.41	0.48
135.22	3.5	0.045	2134.32	0.9	2135.23	1.41	0.17	2.49	38.34	0.47

### Kittitas Conservation District

#### The Ranch at Swauk Creek Diversion Improvement and Restoration Project

**Proposed Conditions** 

River Sta	Q Total	Manning n	Min Ch El	Max Chi Dpth	W.S. Elev	Vel Chnl	Shear Chan	Flow Area	Top Width	Froude # Chl
	(cfs)		(ft)	(ft)	(ft)	(ft/s)	(lb/sq ft)	(sq ft)	(ft)	
7165.97	1180	0.045	2218.25	4.24	2222.49	4.65	0.84	309.59	172.08	0.45
7165.97	498	0.045	2218.25	3.27	2221.52	4.99	1.08	102.03	114.33	0.58
7165.97	356	0.045	2218.25	2.88	2221.13	4.33	0.87	82.69	93.11	0.55
7165.97	264	0.045	2218.25	2.59	2220.84	3.79	0.7	69.77	83.79	0.52
7165.97	4.6	0.045	2218.25	0.62	2218.87	0.81	0.06	5.71	19.95	0.27
7165.97	3.5	0.045	2218.25	0.57	2218.82	0.74	0.05	4.74	18.38	0.26
6877.12	1180	0.045	2216.21	3.45	2219.66	8.09	2.6	150.48	78.37	0.82
6877.12	498	0.045	2216.21	2.22	2218.44	5.81	1.59	85.84	48.31	0.76
6877.12	356	0.045	2216.21	1.88	2218.09	5.14	1.34	69.23	47.11	0.75
6877.12	264	0.045	2216.21	1.59	2217.8	4.72	1.2	55.93	46.13	0.76
6877.12	4.6	0.045	2216.21	0.19	2216.4	1.87	0.42	2.46	22.61	
6877.12	3.5	0.045	2216.21	0.17	2216.38	1.75	0.39	2	21.69	1.02
6650.42	1180	0.045	2213.29	3.75	2217.04	7.35	2.11	172.38	74.53	0.72
6650.42	+		2213.29			5.12		97.9	51.78	0.63
6650.42			2213.29		2215.53	4.46	0.96	79.79	47.5	
6650.42			2213.29		2215.21	4.03	0.82	65.5	43.84	0.58
6650.42	4.6	0.045	2213.29	0.28	2213.57	0.76	0.06	6.07	30.46	0.3
6650.42	3.5	0.045	2213.29	0.25	2213.54	0.67	0.05	5.23	30.32	0.28
6424.86	1180	0.045	2210.75	4.9	2215.65	5.89	1.26	226.35	84.74	0.52
6424.86						5.06				
6424.86						4.56	0.97	78.44	44.25	
6424.86	-				-	4.21	0.88	62.67	40.75	
6424.86					-	2.14		2.15		
6424.86	-		-		-	2.09	0.51	1.68	14.68	1.09

5050.04	4400	0.045	2222 7							
6259.81	1180	0.045	2209.7	4.25	2213.95	8	2.37	151.94	46.24	0.73
6259.81	498	0.045	2209.7	3.35	2213.05	4.49	0.82	112.33	42.52	0.47
6259.81	356	0.045	2209.7	2.98	2212.68	3.7	0.58	96.81	40.95	0.41
6259.81	264	0.045	2209.7	2.67	2212.37	3.13	0.44	84.37	39.6	0.37
6259.81	4.6	0.045	2209.7	0.51	2210.21	0.48	0.02	9.54	28.84	0.15
6259.81	3.5	0.045	2209.7	0.46	2210.16	0.42	0.02	8.28	28.58	0.14
6079.35	1180	0.045	2209.43	2.62	2212.05	6.19	1.77	221.27	194.05	0.79
6079.35	498	0.045	2209.43	1.74	2211.17	5.64	1.8	89.08	88.9	0.79
6079.35	356	0.045	2209.43	1.52	2210.95	5.15	1.63	69.54	87.34	1.01
6079.35	264	0.045	2209.43	1.35	2210.93	4.79	1.65	55.31	80.45	
6079.35	4.6	0.045	2209.43	0.21	2210.78	1.62	0.33	2.83	30.53	1.01 0.94
6079.35	3.5	0.045	2209.43	0.21	2209.62	1.54	0.33	2.83	30.33	0.94
0075.55	5.5	0.045	2203.43	0.15	2203.02	1.54	0.52	2.20	30.21	0.33
5902.35	1180	0.045	2205.98	3.45	2209.43	5.23	1.13	257.89	148.45	0.56
5902.35	498	0.045	2205.98	2.57	2208.55	3.88	0.71	141.77	113.12	0.51
5902.35	356	0.045	2205.98	2.25	2208.23	3.57	0.63	108.36	98.42	0.51
5902.35	264	0.045	2205.98	2.03	2208.01	3.17	0.52	88.1	85.71	0.48
5902.35	4.6	0.045	2205.98	0.53	2206.51	0.58	0.03	7.86	32.19	0.21
5902.35	3.5	0.045	2205.98	0.48	2206.46	0.54	0.03	6.53	30.21	0.2
5773.55	1180	0.045	2205.46	2.07	2207.53	6.9	2.34	171.97	112.7	0.97
5773.55	498	0.045	2205.46	1.39	2206.85	5.09	1.53	97.76	106.67	0.94
5773.55	356	0.045	2205.46	1.28	2206.74	4.14	1.05	85.9	105.37	0.81
5773.55	264	0.045	2205.46	1.13	2206.59	3.79	0.94	69.65	103.63	0.82
5773.55	4.6	0.045	2205.46	0.23	2205.69	1.86	0.43	2.47	24.36	1.03
5773.55	3.5	0.045	2205.46	0.21	2205.67	1.82	0.4	1.92	18.74	1
5598.93	1180	0.045	2201.13	3.35	2204.48	7.13	2.11	167.65	71.03	0.78
5598.93	498	0.045	2201.13	2.22	2203.35	5.3	1.41	94.03	63.34	0.76
5598.93	356	0.045	2201.13	1.84	2202.97	5.08	1.43	70.02	62.71	0.85
5598.93	264	0.045	2201.13	1.65	2202.78	4.54	1.2	58.18	60.32	0.81
5598.93	4.6	0.045	2201.13	0.31	2201.44	1.04	0.11	4.41	22.22	0.41
5598.93	3.5	0.045	2201.13	0.28	2201.41	0.92	0.09	3.79	21.39	0.39

5245.6	1180	0.045	2194.98	4.71	2199.69	8.91	2.88	150.63	95.19	0.78
5245.6	498	0.045	2194.98	3.05	2198.03	6.7	1.94	74.44	31.92	0.76
5245.6	356	0.045	2194.98	2.73	2197.71	5.53	1.39	64.35	30.68	0.67
5245.6	264	0.045	2194.98	2.25	2197.23	5.25	1.32	50.24	28.11	0.69
5245.6	4.6	0.045	2194.98	0.22	2195.2	1.94	0.43	2.37	18.48	0.95
5245.6	3.5	0.045	2194.98	0.19	2195.17	1.88	0.43	1.86	18.33	1.04
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5069.13	1180	0.045	2192.22	3.96	2196.19	11.6	5.17	130.38	82.98	1.09
5069.13	498	0.045	2192.22	3.17	2195.39	7.6	2.41	75.01	53.39	0.81
5069.13	356	0.045	2192.22	2.59	2194.81	7.35	2.44	50.66	33.85	0.88
5069.13	264	0.045	2192.22	2.34	2194.56	6.27	1.85	42.71	28.97	0.8
5069.13	4.6	0.045	2192.22	0.61	2192.83	0.62	0.03	7.41	18.01	0.17
5069.13	3.5	0.045	2192.22	0.57	2192.79	0.53	0.02	6.63	17.69	0.15
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5043.89	1180	0.045	2192.55	4.01	2196.56	7.39	2.03	178.6	66.78	0.67
5043.89	498	0.045	2192.55	2.64	2195.19	5.74	1.43	93.62	55.88	0.65
5043.89	356	0.045	2192.55	2.16	2194.71	5.37	1.34	68.64	46.01	0.68
5043.89	264	0.045	2192.55	1.8	2194.35	4.95	1.22	53.44	36.72	0.69
5043.89	4.6	0.045	2192.55	0.13	2192.68	1.88	0.44	2.45	25.42	1.07
5043.89	3.5	0.045	2192.55	0.12	2192.67	1.64	0.35	2.13	25.37	1
4997.51	1180	0.045	2191.29	5.15	2196.44	5.94	1.23	218.98	71.9	0.48
4997.51	498	0.045	2191.29	3.9	2195.19	3.6	0.5	144.04	52.86	0.34
4997.51	356	0.045	2191.29	3.43	2194.72	3.03	0.37	120.37	49.24	0.31
4997.51	264	0.045	2191.29	3.08	2194.37	2.56	0.28	103.9	42.86	0.28
4997.51	4.6	0.045	2191.29	0.83	2192.12	0.26	0.01	17.5	35.83	0.07
4997.51	3.5	0.045	2191.29	0.74	2192.03	0.24	0	14.5	35.67	0.07
4969.06	1180	0.045	2189.69	6.77	2196.46	5	0.81	265.81	65.13	0.36
4969.06	498	0.045	2189.69	5.5	2195.19	2.85	0.29	189.93	55.52	0.23
4969.06	356	0.045	2189.69	5.04	2194.73	2.32	0.19	164.62	52.94	0.2
4969.06	264	0.045	2189.69	4.68	2194.37	1.9	0.13	147.15	46.93	0.17
4969.06	4.6	0.045	2189.69	2.43	2192.12	0.08	0	55.04	35.52	0.01

4969.06	3.5	0.045	2189.69	2.34	2192.03	0.07	0	52.08	35.18	0.01
4965.06	1180	0.045	2191.5	3.96	2195.46	9.27	3.47	135.52	57.12	0.96
4965.06	498	0.045	2191.5	3.41	2194.91	5.02	1.09	104.93	54.61	0.58
4965.06	356	0.045	2191.5	2.98	2194.48	4.51	0.94	82.31	49.82	0.58
4965.06	264	0.045	2191.5	2.64	2194.15	4.14	0.85	66.11	48.16	0.58
4965.06	4.6	0.045	2191.5	0.55	2192.05	1.95	0.3	2.36	5.97	0.55
4965.06	3.5	0.045	2191.5	0.48	2191.98	1.82	0.27	1.93	5.5	0.54
4943.6	1180	0.045	2191	4.82	2195.42	7.01	1.93	175.36	61.95	0.7
4943.6	498	0.045	2191	3.54	2194.14	7.39	2.55	69.49	42.28	0.95
4943.6	356	0.045	2191	3.17	2193.78	6.68	2.24	54.34	39.97	0.96
4943.6	264	0.045	2191	2.95	2193.55	5.89	1.85	45.37	38.54	0.92
4943.6	4.6	0.045	2191	0.94	2191.54	3.02	0.75	1.52	4.4	0.9
4943.6	3.5	0.045	2191	0.88	2191.48	2.77	0.66	1.26	4.04	0.87
4908.09	1180	0.045	2190.07	4.8	2194.39	8.83	3.31	134.88	56.27	0.99
4908.09	498	0.045	2190.07	3.43	2193.02	7.8	3.15	63.94	47.17	1.17
4908.09	356	0.045	2190.07	3.22	2192.81	6.56	2.33	54.29	45.79	1.06
4908.09	264	0.045	2190.07	3.03	2192.62	5.75	1.88	45.89	44.56	1
4908.09	4.6	0.045	2190.07	1.15	2190.74	2.28	0.41	2.02	5.02	0.63
4908.09	3.5	0.045	2190.07	1.07	2190.66	2.16	0.38	1.62	4.52	0.64
4871.2	1180	0.045	2189.43	4.19	2193.62	7.11	1.91	171.39	56.93	0.66
4871.2	498	0.045	2189.43	2.71	2192.14	5.22	1.23	95.38	46.13	0.64
4871.2	356	0.045	2189.43	2.22	2191.65	4.84	1.13	73.57	42.84	0.65
4871.2	264	0.045	2189.43	1.84	2191.27	4.59	1.08	57.56	40.24	0.68
4871.2	4.6	0.045	2189.43	0.2	2189.63	2.12	0.53	2.17	18.36	1.09
4871.2	3.5	0.045	2189.43	0.18	2189.61	1.79	0.38	1.96	17.63	0.95
4847.25	1180	0.045	2189.05	4.72	2193.77	4.95	0.89	246.2	73.94	0.44
4847.25	498	0.045	2189.05	3.11	2192.16	3.57	0.55	139.58	59.53	0.41
4847.25	356	0.045	2189.05	2.59	2191.65	3.24	0.48	109.85	55.14	0.4
4847.25	264	0.045	2189.05	2.19	2191.24	3	0.43	88.13	51.69	0.4

4847.25	4.6	0.045	2189.05	0.34	2189.39	0.65	0.04	7.03	35.97	0.26
4847.25	3.5	0.045	2189.05	0.31	2189.36	0.58	0.03	6.04	35.73	0.25
4775.33	1180	0.045	2188.71	4.09	2192.71	8.1	2.46	163.48	73.67	0.74
4775.33	498	0.045	2188.71	2.82	2191.44	5.62	1.36	89.26	38.79	0.63
4775.33	356	0.045	2188.71	2.39	2191.01	4.87	1.09	73.19	36.08	0.6
4775.33	264	0.045	2188.71	2.03	2190.65	4.35	0.91	60.68	33.95	0.57
4775.33	4.6	0.045	2188.71	0.33	2188.95	1.01	0.11	4.55	30.96	0.46
4775.33	3.5	0.045	2188.71	0.3	2188.92	0.93	0.1	3.75	30.87	0.47
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4646.06	1180	0.045	2187.16	3.53	2190.69	8.92	3.16	141.2	68.53	0.88
4646.06	498	0.045	2187.16	2	2189.16	7.42	2.68	67.08	39.18	1
4646.06	356	0.045	2187.16	1.66	2188.82	6.6	2.26	53.92	38.8	0.99
4646.06	264	0,045	2187.16	1.43	2188.59	5.86	1.88	45.09	38.54	0.95
4646.06	4.6	0.045	2187.16	0.32	2187.48	1.04	0.11	4.41	26.25	0.45
4646.06	3.5	0.045	2187.16	0.29	2187.45	0.92	0.09	3.8	25.67	0.42
4540.24	1180	0.045	2185.06	3.94	2189	7.62	2.2	161.67	56.71	0.72
4540.24	498	0.045	2185.06	2.55	2187.61	5.49	1.35	90.89	44.06	0.66
4540.24	356	0.045	2185.06	2.14	2187.2	4.85	1.12	73.45	41.31	0.64
4540.24	264	0.045	2185.06	1.67	2186.73	4.84	1.2	54.59	38.81	0.72
4540.24	4.6	0.045	2185.06	0.16	2185.22	1.77	0.38	2.6	24.3	0.95
4540.24	3.5	0.045	2185.06	0.14	2185.2	1.72	0.38	2.04	23.74	1.04
4447.62	1180	0.045	2183.23	4.77	2188	7.71	2.26	157.77	52.02	0.72
4447.62	498	0.045	2183.23	3.24	2186.48	5.84	1.56	85.37	43.21	0.72
4447.62	356	0.045	2183.23	2.78	2186.02	5.38	1.41	66.2	38.97	0.73
4447.62	264	0.045	2183.23	2.25	2185.48	5.25	1.3	50.31	26.97	0.68
4447.62	4.6	0.045	2183.23	0.4	2183.64	0.83	0.06	5.51	21.46	0.29
4447.62	3.5	0.045	2183.23	0.37	2183.6	0.74	0.05	4.75	21.35	0.28
4321.17	1180	0.045	2182.22	4.93	2187.15	6.59	1.56	183.16	48.83	0.57
4321.17	498	0.045	2182.22	3.16	2185.38	4.92	1.05	101.29	43.03	0.56
4321.17	356	0.045	2182.22	2.61	2184.83	4.51	0.93	78.96	38.95	0.56

4321.17	264	0.045	2182.22	2.16	2184.38	4.25	0.86	62.17	34.2	0.56
4321.17	4.6	0.045	2182.22	0.23	2182.45	1.49	0.27	3.08	28.42	0.8
4321.17	3.5	0.045	2182.22	0.21	2182.43	1.42	0.26	2.47	27.64	0.84
4177.43	1180	0.045	2180.64	4.6	2185.24	9.11	3.07	135.05	42.38	0.81
4177.43	498	0.045	2180.64	3.1	2183.74	6.41	1.78	77.9	33.84	0.72
4177.43	356	0.045	2180.64	2.66	2183.3	5.6	1.44	63.54	30.67	0.69
4177.43	264	0.045	2180.64	2.29	2182.93	5.02	1.2	52.6	28.45	0.65
4177.43	4.6	0.045	2180.64	0.36	2181	0.86	0.07	5.34	22.21	0.31
4177.43	3.5	0.045	2180.64	0.33	2180.97	0.77	0.06	4.57	22.14	0.3
4050.15	1180	0.045	2179.81	4.74	2184.55	6.54	1.55	188.17	59.03	0.57
4050.15	498	0.045	2179.81	2.9	2182.71	5.05	1.1	99.01	42.29	0.57
4050.15	356	0.045	2179.81	2.39	2182.2	4.55	0.95	78.32	39.79	0.57
4050.15	264	0.045	2179.81	2.02	2181.83	4.13	0.83	63.91	37.75	0.56
4050.15	4.6	0.045	2179.81	0.19	2180	1.12	0.14	4.11	29.43	0.53
4050.15	3.5	0.045	2179.81	0.17	2179.98	1.02	0.12	3.43	29.35	0.53
4019.45	1180	0.045	2179.46	4.75	2184.21	7.08	1.81	170.64	46.86	0.61
4019.45	498	0.045	2179.46	2.97	2182.43	5.26	1.19	94.63	38.59	0.59
4019.45	356	0.045	2179.46	2.47	2181.93	4.69	1.01	75.88	37.04	0.58
4019.45	264	0.045	2179.46	2.11	2181.57	4.23	0.86	62.43	36.15	0.57
4019.45	4.6	0.045	2179.46	0.31	2179.77	0.79	0.06	5.81	27.32	0.3
4019.45	3.5	0.045	2179.46	0.27	2179.73	0.73	0.05	4.82	26.83	0.3
3989.98	1180	0.045	2179.22	3.79	2183.01	10.06	3.94	119.27	40.27	0.97
3989.98	498	0.045	2179.22	2.22	2181.44	7.93	2.93	62.8	32.62	1.01
3989.98	356	0.045	2179.22	1.81	2181.03	7.17	2.56	49.63	31.36	1.01
3989.98	264	0.045	2179.22	1.5	2180.72	6.57	2.27	40.19	30.12	1
3989.98	4.6	0.045	2179.22	0.13	2179.35	2.03	0.52	2.26	23.98	1.17
3989.98	3.5	0.045	2179.22	0.12	2179.34	1.68	0.36	2.08	23.94	1
3957.3	1180	0.045	2177.27	3.29	2180.56	13.58	7.96	86.91	34.97	1.52
3957.3	498	0.045	2177.27	2.15	2179.42	10.42	5.57	47.8	33.28	1.53

3957.3	356	0.045	2177.27	1.86	2179.14	9.27	4.71	38.42	32.85	1.51
3957.3	264	0.045	2177.27	1.66	2178.93	8.29	4	31.83	32.53	1.48
3957.3	4.6	0.045	2177.27	0.29	2177.56	1.75	0.31	2.63	14.74	0.73
3957.3	3.5	0.045	2177.27	0.26	2177.53	1.6	0.27	2.19	14.35	0.72
3929.03	1180	0.045	2176.05	6.12	2182.17	5.51	1.04	229.68	63.67	0.44
3929.03	498	0.045	2176.05	3.75	2179.8	4.76	0.96	104.67	40.23	0.52
3929.03	356	0.045	2176.05	3.1	2179.16	4.49	0.92	79.36	38.46	0.55
3929.03	264	0.045	2176.05	2.6	2178.65	4.39	0.95	60.1	37.7	0.61
3929.03	4.6	0.045	2176.05	0.39	2176.44	2.48	0.61	1.86	9.7	1
3929.03	3.5	0.045	2176.05	0.35	2176.4	2.42	0.59	1.44	7.92	1
3894.78	1180	0.045	2174.56	7.16	2181.71	7.07	1.62	178.67	36.03	0.5
3894.78	498	0.045	2174.56	5.1	2179.65	4.71	0.83	109.58	31.02	0.41
3894.78	356	0.045	2174.56	4.48	2179.04	4.02	0.63	91	29.52	0.38
3894.78	264	0.045	2174.56	4	2178.56	3.49	0.5	77.02	28.35	0.36
3894.78	4.6	0.045	2174.56	1.21	2175.77	0.26	0	17.48	16.95	0.05
3894.78	3.5	0.045	2174.56	1.17	2175.72	0.21	0	16.67	16.91	0.04
3866.61	1180	0.045	2174	7.59	2181.59	6.95	1.56	178.56	34.25	0.48
3866.61	498	0.045	2174	5.59	2179.59	4.4	0.71	115.35	29.4	0.37
3866.61	356	0.045	2174	4.99	2178.99	3.67	0.52	98.03	27.98	0.33
3866.61	264	0.045	2174	4.51	2178.51	3.12	0.39	85.04	26.69	0.3
3866.61	4.6	0.045	2174	1.77	2175.77	0.19	0	24.52	18.32	0.03
3866.61	3.5	0.045	2174	1.72	2175.72	0.15	0	23.65	18.21	0.02
3843.82	1180	0.045	2175.35	5.74	2181.09	8.32	2.38	146.21	33.95	0.65
3843.82	498	0.045	2175.35	3.95	2179.3	5.52	1.21	90.28	28.26	0.54
3843.82	356	0.045	2175.35	3.4	2178.75	4.73	0.94	75.21	26.6	0.5
3843.82	264	0.045	2175.35	2.96	2178.31	4.13	0.74	63.89	25.23	0.46
3843.82	4.6	0.045	2175.35	0.41	2175.76	0.62	0.03	7.47	19.28	0.17
3843.82	3.5	0.045	2175.35	0.37	2175.72	0.53	0.02	6.6	19.18	0.16
3803.77	1180	0.045	2175.34	5.28	2180.62	8.75	2.67	141.38	36.15	0.71

0.59	30.03	85.85	1.38	5.86	2178.96	3.61	2175.34	0.045	498	3803.77
0.56	28.52	70.87	1.09	5.05	2178.44	3.1	2175.34	0.045	356	3803.77
0.53	27.5	59.26	0.9	4.46	2178.03	2.69	2175.34	0.045	264	3803.77
0.33	20.17	4.92	0.08	0.93	2175.66	0.32	2175.34	0.045	4.6	3803.77
0.33	20.09	4.17	0.07	0.84	2175.62	0.28	2175.34	0.045	3.5	3803.77
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0.55	47.82	183.25	1.66	6.94	2180.66	5.53	2175.12	0.045	1180	3763.5
0.51	39.25	101.77	1.06	5.16	2178.78	3.66	2175.12	0.045	498	3763.5
0.49	36.57	80.94	0.89	4.59	2178.23	3.11	2175.12	0.045	356	3763.5
0.47	34.36	65.94	0.75	4.12	2177.81	2.69	2175.12	0.045	264	3763.5
0.3	22.73	5.52	0.06	0.83	2175.47	0.35	2175.12	0.045	4.6	3763.5
0.29	22.68	4.69	0.05	0.75	2175.43	0.31	2175.12	0.045	3.5	3763.5
0.66	51.16	159.93	2.15	7.76	2178.72	4.72	2174	0.045	1180	3520.45
0.57	36.8	94.34	1.17	5.31	2177.17	3.17	2174	0.045	498	3520.45
0.55	34.77	76.09	0.97	4.68	2176.66	2.66	2174	0.045	356	3520.45
0.54	33.35	62.73	0.83	4.21	2176.27	2.27	2174	0.045	264	3520.45
0.32	25.29	5.41	0.07	0.85	2174.33	0.33	2174	0.045	4.6	3520.45
0.32	25.12	4.58	0.06	0.76	2174.3	0.3	2174	0.045	3.5	3520.45
0.68	75.31	174.58	2.21	7.86	2177.13	4.47	2172.65	0.045	1180	3328.42
0.6	38.25	90.28	1.32	5.66	2175.68	3.03	2172.65	0.045	498	3328.42
0.57	34.76	73.1	1.06	4.93	2175.2	2.55	2172.65	0.045	356	3328.42
0.55	33.11	60.89	0.88	4.36	2174.84	2.19	2172.65	0.045	264	3328.42
0.47	23.94	4.16	0.13	1.11	2172.88	0.23	2172.65	0.045	4.6	3328.42
0.46	23.76	3.49	0.11	1	2172.85	0.2	2172.65	0.045	3.5	3328.42
0.95	46.27	127.86	3.66	9.72	2172.93	3.67	2169.26	0.045	1180	3027.98
0.96	41	67.61	2.63	7.54	2171.56	2.3	2169.26	0.045	498	3027.98
0.93	38.46	54.17	2.17	6.63	2171.22	1.96	2169.26	0.045	356	3027.98
0.91	34.15	44.59	1.84	5.92	2170.96	1.69	2169.26	0.045	264	3027.98
0.46	18.91	3.9	0.13	1.18	2169.56	0.3	2169.26	0.045	4.6	3027.98
0.44	18.29	3.29	0.12	1.06	2169.52	0.26	2169.26	0.045	3.5	3027.98

2983.9	1180	0.045	2168.33	3.29	2171.62	10.41	4.59	115.32	51.97	1.16
2983.9	498	0.045	2168.33	2.83	2171.16	5.44	1.34	92.04	48.23	0.67
2983.9	356	0.045	2168.33	2.46	2170.79	4.76	1.1	74.82	45.1	0.65
2983.9	264	0.045	2168.33	2.14	2170.47	4.32	0.95	61.04	42	0.63
2983.9	4.6	0.045	2168.33	0.26	2168.6	2.41	0.59	1.91	10.61	1
2983.9	3.5	0.045	2168.33	0.23	2168.56	2.29	0.55	1.53	9.52	1.01
2823.31	1180	0.045	2166.92	4.28	2171.2	5.41	1.12	261.93	140.81	0.52
2823.31	498	0.045	2166.92	3.23	2170.15	4.07	0.72	129.73	91.42	0.48
2823.31	356	0.045	2166.92	2.88	2169.8	3.52	0.57	103.11	62.57	0.45
2823.31	264	0.045	2166.92	2.57	2169.49	3.15	0.48	84.88	55.95	0.43
2823.31	4.6	0.045	2166.92	0.47	2167.39	0.72	0.05	6.43	24.04	0.24
2823.31	3.5	0.045	2166.92	0.43	2167.35	0.64	0.04	5.47	23.53	0.23
2472.76	1180	0.045	2164.51	2.91	2167.42	8.05	2.73	156.47	80.21	0.89
2472.76		0.045		1.78		6.55	2.73	76.75	57.91	0.83
2472.76	498	0.045	2164.51		2166.29					
2472.76	356	0.045	2164.51	1.47	2165.98	6.03	2.01	59.11	54.37	1.01
2472.76	264	0.045	2164.51	1.25	2165.77	5.51	1.77	47.91	49.93	0.99
2472.76	4.6	0.045	2164.51	0.18	2164.69	1.77	0.39	2.61	27.88	1.02
2472.76	3.5	0.045	2164.51	0.16	2164.67	1.68	0.38	2.08	27.1	1.07
2151.63	1180	0.045	2159.74	3.5	2163.24	5.21	1.1	242.45	148	0.55
2151.63	498	0.045	2159.74	2.3	2162.04	3.99	0.78	126.75	84.31	0.55
2151.63	356	0.045	2159.74	2.05	2161.79	3.38	0.59	106.14	81.36	0.51
2151.63	264	0.045	2159.74	1.83	2161.57	3.01	0.49	88.3	78.73	0.49
2151.63	4.6	0.045	2159.74	0.4	2160.14	0.88	0.07	5.24	22.85	0.32
2151.63	3.5	0.045	2159.74	0.34	2160.08	0.87	0.07	4	17.23	0.32
1781.43	1180	0.045	2155.44	3.06	2158.5	8.71	3.22	136.98	59.9	0.97
1781.43	498	0.045	2155.44	2.09	2157.53	6.02	1.78	82.79	52.11	0.84
1781.43	356	0.045	2155.44	1.65	2157.09	5.87	1.84	60.63	48.41	0.92
1781.43	264	0.045	2155.44	1.4	2156.84	5.39	1.64	48.94	46.3	0.93
1781.43	4.6	0.045	2155.44	0.23	2155.67	1.71	0.36	2.69	26.55	0.95
1781.43	3.5	0.045	2155.44	0.21	2155.65	1.63	0.34	2.15	23.76	0.96

1289.9	1180	0.045	2149.26	3.75	2153.01	6.54	1.63	183.09	56.93	0.62
1289.9	498	0.045	2149.26	2.26	2151.52	4.92	1.11	101.42	52.12	0.62
1289.9	356	0.045	2149.26	1.98	2151.24	4.08	0.8	87.32	51.1	0.55
1289.9	264	0.045	2149.26	1.7	2150.96	3.62	0.66	73.02	50.06	0.53
1289.9	4.6	0.045	2149.26	0.28	2149.54	0.69	0.05	6.64	43.14	0.31
1289.9	3.5	0.045	2149.26	0.26	2149.52	0.62	0.04	5.65	42.86	0.3
1002.97	1180	0.045	2145.6	3.24	2148.84	9.32	3.56	127.79	49.29	0.98
1002.97	498	0.045	2145.6	2.23	2147.83	6.19	1.81	80.51	44.6	0.81
1002.97	356	0.045	2145.6	1.69	2147.29	6.25	2.03	56.92	41.91	0.95
1002.97	264	0.045	2145.6	1.42	2147.02	5.74	1.82	45.96	40.59	0.95
1002.97	4.6	0.045	2145.6	0.2	2145.8	1.73	0.38	2.66	28.02	0.99
1002.97	3.5	0.045	2145.6	0.18	2145.78	1.6	0.34	2.19	27.17	1
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719.85	1180	0.045	2142.91	3.66	2146.57	5.25	1.08	241.68	104.26	0.52
719.85	498	0.045	2142.91	2.38	2145.29	4.03	0.76	124.68	71.42	0.52
719.85	356	0.045	2142.91	2.23	2145.14	3.14	0.47	114.14	70.07	0.42
719.85	264	0.045	2142.91	1.97	2144.88	2.75	0.38	96.11	67.41	0.4
719.85	4.6	0.045	2142.91	0.29	2143.2	0.58	0.03	7.96	36.42	0.22
719.85	3.5	0.045	2142.91	0.25	2143.16	0.52	0.03	6.72	35.27	0.21
460	1180	0.045	2141.32	2.12	2143.44	7.55	2.68	159.61	135.2	0.99
460	498	0.045	2141.32	1.63	2142.95	4.44	1.03	112.98	89.89	0.68
460	356	0.045	2141.32	1.12	2142.44	5.12	1.6	69.53	83.67	0.99
460	264	0.045	2141.32	0.97	2142.29	4.66	1.4	56.71	81.06	0.98
460	4.6	0.045	2141.32	0.21	2141.53	1.43	0.27	3.23	38.56	0.87
460	3.5	0.045	2141.32	0.19	2141.51	1.33	0.24	2.64	35.58	0.86
135.22	1180	0.045	2134.32	2.99	2137.31	4.39	0.96	269.52	178.9	0.62
135.22	498	0.045	2134.32	2.56	2136.88	5.8	1.88	85.86	162.73	0.98
135.22	356	0.045	2134.32	2.69	2137.01	3.71	0.74	96.09	164.62	0.6
135.22	264	0.045	2134.32	2.48	2136.8	3.31	0.63	79.78	161.69	0.58
135.22	4.6	0.045	2134.32	0.96	2135.28	1.54	0.2	3	39.41	0.48
135.22	3.5	0.045	2134.32	0.9	2135.23	1.41	0.17	2.49	38.34	0.47

## Kittitas Conservation District

## The Ranch at Swauk Creek Diversion Improvement and Restoration Project

**Proposed Conditions - Low Flow** 

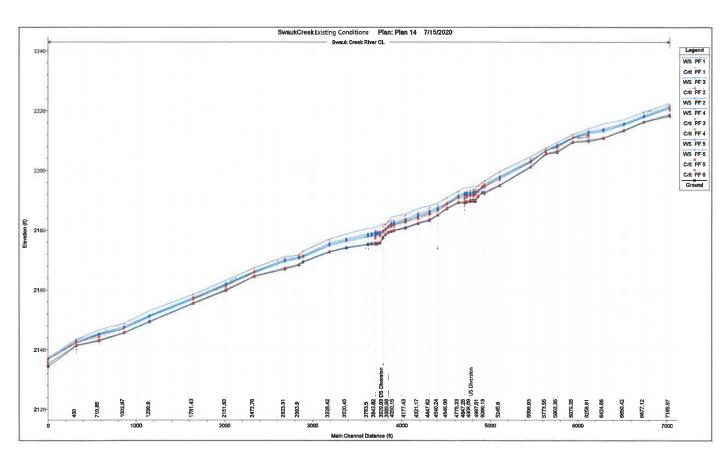
River Sta	Q Total	Manning n	Min Ch El	Max Chl Dpth	W.S. Elev	Vel Chnl	Shear Chan	Flow Area	Top Width	Froude # Chl
	(cfs)		(ft)	(ft)	(ft)	(ft/s)	(lb/sq ft)	(sq ft)	(ft)	
7165.97	4.6	0.25	2218.25	1.08	2219.33	0.28	0.16	16.7	27.36	0.06
7165.97	3.5	0.25	2218.25	0.99	2219.24	0.24	0.13	14.37	26.11	0.06
6877.12	4.6	0.25	2216.21	0.43	2216.64	0.5	0.67	9.18	31.07	0.16
6877.12	3.5	0.25	2216.21	0.35	2216.56	0.52	0.76	6.78	28.5	0.19
6650.42	4.6	0.25	2213.29	0.59	2213.88	0.29	0.19	15.94	32.09	0.07
6650.42	3.5	0.25	2213.29	0.53	2213.82	0.25	0.14	14.03	31.78	0.07
6424.86	4.6	0.25	2210.75	0.58	2211.33	0.55	0.72	8.36	20.22	0.15
6424.86	3.5	0.25	2210.75	0.47	2211.22	0.57	0.83	6.19	19.25	0.18
6259.81	4.6	0.25	2209.7	0.99	2210.69	0.19	0.07	24.21	31.68	0.04
6259.81	3.5	0.25	2209.7	0.89	2210.59	0.17	0.06	20.92	31.02	0.04
6079.35	4.6	0.25	2209.43	0.21	2209.64	1.62	10.29	2.83	30.53	0.94
6079.35	3.5	0.25	2209.43	0.19	2209.62	1.54	9.88	2.28	30.21	0.99
5902.35	4.6	0.25	2205.98	0.92	2206.9	0.2	0.09	22.96	42.7	0.09
5902.35	3.5	0.25	2205.98	0.85	2206.83	0.18	0.07	19.86	41.26	0.04
5773.55	4.6	0.25	2205.46	0.33	2205.79	0.79	2.14	5.85	44.2	0.38
5773.55	3.5	0.25	2205.46	0.22	2205.69	1.51	8.65	2.32	22.79	0.84
5598.93	4.6	0.25	2201.13	0.67	2201.8	0.32	0.23	14.45	30.83	0.08
5598.93	3.5	0.25	2201.13	0.62	2201.75	0.27	0.17	12.91	30.2	0.0
5245.6	4.6	0.25	2194.98	0.42	2195.4	0.75	1.48	6.11	19.56	0.24

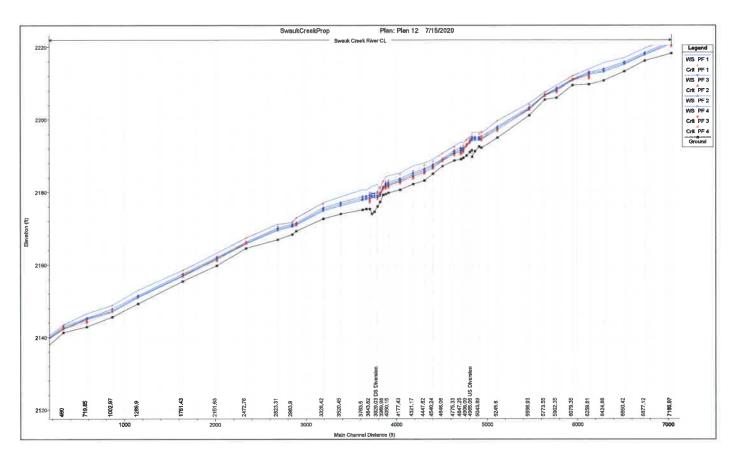
5245.6	3.5	0.25	2194.98	0.31	2195.29	0.88	2.3	3.99	18.95	0.34
	1.0	1								
5069.13	4.6	0.25	2192.22	0.96	2193.18	0.33	0.22	13.79	19.01	0.07
5069.13	3.5	0.25	2192.22	0.88	2193.1	0.28	0.17	12.29	18.85	0.06
5043.89	4.6	0.25	2192.55	0.28	2192.83	0.73	1.53	6.27	26.06	0.26
5043.89	3.5	0.25	2192.55	0.14	2192.69	1.29	6.26	2.7	25.47	0.7
4997.51	4.6	0.25	2191.29	1.5	2192.79	0.11	0.02	41.89	37.08	0.02
4997.51	3.5	0.25	2191.29	1.38	2192.67	0.09	0.02	37.4	36.85	0.02
4969.06	4.6	0.25	2189.69	3.09	2192.79	0.05	0	79.62	38.29	0.01
4969.06	3.5	0.25	2189.69	2.97	2192.66	0.04	0	75.02	37.72	0.01
4965.06	4.6	0.25	2191.5	1.28	2192.78	0.45	0.48	10.24	24.03	0.12
4965.06	3.5	0.25	2191.5	1.16	2192.66	0.45	0.48	7.73	17.44	0.12
4943.6	4.6	0.25	2191	1.76	2192.36	0.54	0.65	8.58	17.29	0.13
4943.6	3.5	0.25	2191	1.62	2192.22	0.54	0.67	6.42	13.34	0.14
4908.09	4.6	0.25	2190.07	1.66	2191.25	0.81	1.49	5.68	11.68	0.2
4908.09	3.5	0.25	2190.07	1.58	2191.17	0.73	1.19	4.82	9.57	0.18
4871.2	4.6	0.25	2189.43	0.49	2189.92	0.47	0.56	9.81	29.58	0.14
4871.2	3.5	0.25	2189.43	0.42	2189.85	0.45	0.55	7.83	29.4	0.15
4847.25	4.6	0.25	2189.05	0.65	2189.7	0.24	0.13	18.82	38.67	0.06
4847.25	3.5	0.25	2189.05	0.58	2189.63	0.22	0.11	16.15	38.08	0.06
4775.33	4.6	0.25	2188.71	0.61	2189.23	0.34	0.28	13.4	31.99	0.09
4775.33	3.5	0.25	2188.71	0.53	2189.15	0.32	0.25	11.03	31.72	0.09
4646.06	4.6	0.25	2187.16	0.6	2187.76	0.34	0.28	13.69	36.57	0.:
4646.06	3.5	0.25	2187.16	0.55	2187.71	0.29	0.22	11.88	35.19	0.09

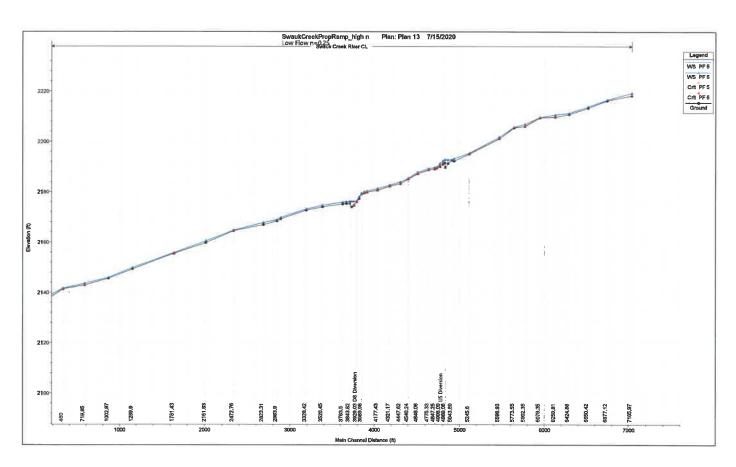
4540.24	4.6	0.25	2185.06	0.36	2185.42	0.57	0.89	8.12	31.29	0.
4540.24	3.5	0.25	2185.06	0.29	2185.35	0.57	0.97	6.13	29.67	0.2
4447.62	4.6	0.25	2183.23	0.75	2183.99	0.35	0.26	13.21	22.58	0.0
4447.62	3.5	0.25	2183.23	0.68	2183.91	0.31	0.21	11.43	22.33	0.0
4321.17	4.6	0.25	2182.22	0.54	2182.76	0.38	0.35	11.98	29.46	0.1
4321.17	3.5	0.25	2182.22	0.47	2182.69	0.35	0.32	9.86	29.33	0.1
7021.17	5.5	0.25	2102.21	0.17	2202,00	4.55	5.02	5.55		
4177.43	4.6	0.25	2180.64	0.71	2181.35	0.35	0.26	13.26	22.91	0.0
4177.43	3.5	0.25	2180.64	0.63	2181.27	0.31	0.21	11.38	22.74	0.0
4050.15	4.6	0.25	2179.81	0.52	2180.33	0.33	0.26	13.82	30.36	0.0
4050.15	3.5	0.25	2179.81	0.44	2180.25	0.3	0.23	11.49	30.16	0.0
4019.45	4.6	0.25	2179.46	0.62	2180.09	0.31	0.22	14.79	29.14	0.0
4019.45	3.5	0.25	2179.46	0.56	2180.02	0.27	0.17	12.91	28.99	0.0
3989.98	4.6	0.25	2179.22	0.19	2179.41	1.23	5	3.74	24.34	0.5
3989.98	3.5	0.25	2179.22	0.15	2179.37	1.25	5.62	2.81	24.11	0.6
3957.3	4.6	0.25	2177.27	0.71	2177.98	0.47	0.49	9.81	18.9	0.1
3957.3	3.5	0.25	2177.27	0.62	2177.9	0.42	0.41	8.31	18.44	0.1
3929.03	4.6	0.25	2176.05	0.39	2176.44	2.48	18.83	1.86	9.7	
3929.03	3.5	0.25	2176.05	0.35	2176.4	2.42	18.32	1.44	7.92	
	-									
3894.78	4.6	0.25	2174.56	1.72	2176.28	0.18	0.05	26.27	17.51	0.0
3894.78	3.5	0.25	2174.56	1.6	2176.16	0.14	0.03	24.17	17.36	0.0
3866.61	4.6	0.25	2174	2.27	2176.27	0.14	0.03	33.98	19.61	0.0
3866.61	3.5	0.25	2174	2.15	2176.15	0.11	0.02	31.7	19.27	0.0

3843.82	4.6	0.25	2175.35	0.9	2176.25	0.27	0.13	17.22	20.36	0.05
3843.82	3.5	0.25	2175.35	0.79	2176.14	0.23	0.11	14.92	20.11	0.05
3803.77	4.6	0.25	2175.34	0.77	2176.11	0.32	0.21	14.24	21.13	0.07
3803.77	3.5	0.25	2175.34	0.66	2176	0.29	0.18	12.02	20.91	0.07
3763.5	4.6	0.25	2175.12	0.81	2175.93	0.29	0.17	16	23.35	0.06
3763.5	3.5	0.25	2175.12	0.7	2175.82	0.26	0.14	13.53	23.21	0.06
3520.45	4.6	0.25	2174	0.68	2174.68	0.32	0.22	14.55	27.11	0.08
3520.45	3.5	0.25	2174	0.6	2174.6	0.28	0.18	12.46	26.71	0.07
3328.42	4.6	0.25	2172.65	0.58	2173.23	0.35	0.28	13.09	26.09	0.09
3328.42	3.5	0.25	2172.65	0.58	2173.25	0.32	0.25	10.83	25.64	0.09
									v	
3027.98	4.6	0.25	2169.26	0.63	2169.89	0.4	0.38	11.49	27.36	0.11
3027.98	3.5	0.25	2169.26	0.57	2169.83	0.35	0.31	9.94	26.84	0.1
2983.9	4.6	0.25	2168.33	0.65	2168.98	0.51	0.66	9.02	26.68	0.15
2983.9	3.5	0.25	2168.33	0.56	2168.89	0.52	0.73	6.71	23.2	0.17
2823.31	4.6	0.25	2166.92	0.94	2167.86	0.24	0.12	18.83	29.07	0.05
2823.31	3.5	0.25	2166.92	0.84	2167.76	0.22	0.1	16.13	28.11	0.05
2472.76	4.6	0.25	2164.51	0.33	2164.84	0.62	1.13	7.46	35.45	0.24
2472.76	3.5	0.25	2164.51	0.28	2164.79	0.62	1.25	5.61	33.85	0.27
2151.63	4.6	0.25	2159.74	0.78	2160.52	0.23	0.13	19.63	48.55	0.06
2151.63	3.5	0.25	2159.74	0.72	2160.46	0.21	0.11	16.59	45.56	0.06
1781.43	4.6	0.25	2155.44	0.4	2155.84	0.59	0.99	7.79	31.89	0.21
1781.43	3.5	0.25	2155.44	0.34	2155.78	0.58	1.02	6.05	30.86	0.23
1289.9	4.6	0.25	2149.26	0.57	2149.83	0.24	0.13	19.24	44.67	0.06
1200.0		5.25	22 15.20	0.57	22 ,5.05	0.27	0.10	17:67	77.07	0.00

1289.9	3.5	0.25	2149.26	0.51	2149.77	0.21	0.11	16.61	44.36	0.06
1002.97	4.6	0.25	2145.6	0.34	2145.94	0.7	1.45	6.56	30.08	0.26
1002.97	3.5	0.25	2145.6	0.28	2145.88	0.71	1.6	4.93	28.6	0.3
719.85	4.6	0.25	2142.91	0.64	2143.55	0.2	0.09	22.97	45.78	0.05
719.85	3.5	0.25	2142.91	0.57	2143.48	0.18	0.07	19.61	45.08	0.05
460	4.6	0.25	2141.32	0.37	2141.69	0.4	0.5	11.41	60.34	0.16
460	3.5	0.25	2141.32	0.34	2141.66	0.37	0.44	9.48	58.54	0.16
135.22	4.6	0.25	2134.32	1.48	2135.8	0.35	0.28	13.32	76.15	0.09
135.22	3.5	0.25	2134.32	1.4	2135.72	0.32	0.25	10.91	71.62	0.09







# Appendix E Fish Screen Information



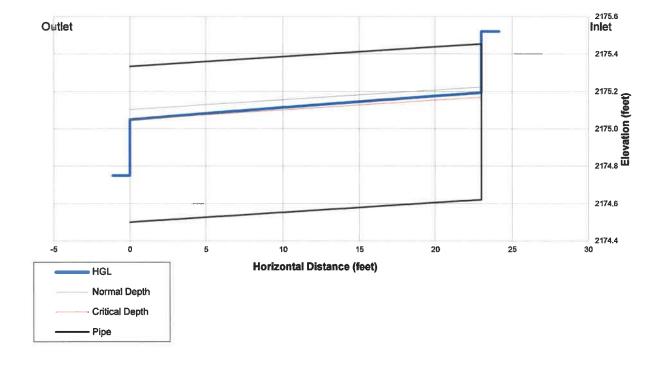
The 24" diameter by 6' length modular drum screen has a max diversion amount of ~3.6 cfs.

# Appendix F Delivery Pipeline Hydraulic Analysis

System: The Ranch at Swauk Creek

Reach: Burke Road Pipeline, MH #3 to Ditch

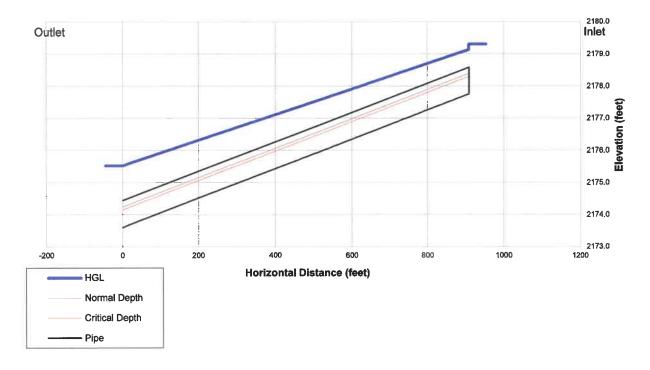
	<u>Outlet</u>	<u>Inlet</u>		
Identification	DITCH	MH #3	Normal Depth (ft)	0.60
Station	28+10	27+87	Critical Depth (ft)	0.55
Rim/Overflow Elev. (ft)	2176.00	2177.10	Froude No.	0.83
Invert Elevation (ft)	2174.50	2174.62	Avg. Velocity (fps)	3.83
Water Surf. Elev. (ft)	2174.75	2175.52	Min. Velocity (fps)	3.75
			Max. Velocity (fps)	3.94
Discharge (cfs)	1.50		Normal Velocity (fps)	3.55
Diameter (inches)	10		Crit. Velocity (fps)	3.94
Ineffective Depth(ft)	0.00			
Length (feet)	23.0		freeboard @ outlet	1.25
Manning n	0.012		freeboard @ inlet	1.58
Entrance Vel. (fps)	0.00			
Entrance Loss (Ke)	0.50		Normal EGL (ft)	0.80
Slope	0.0052		Hyd.Jump d/s E	0.80



System: The Ranch at Swauk Creek

Reach: Burke Road Pipeline, MH #2 to MH #3 (Crosses Swauk Creek)

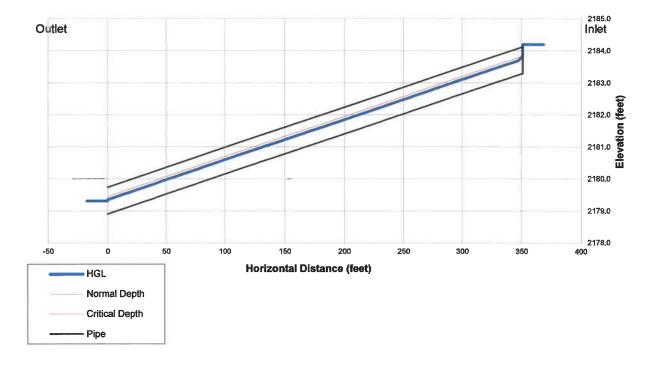
	<u>Outlet</u>	<u>Inlet</u>		
Identification	MH #3	MH #2	Normal Depth (ft)	0.64
Station	27+83	18+74	Critical Depth (ft)	0.55
Rim/Overflow Elev. (ft)	2177.10	2181.75	Froude No.	0.74
Invert Elevation (ft)	2173.60	2177.75	Avg. Velocity (fps)	2.75
Water Surf. Elev. (ft)	2175.52	2179,31	Min. Velocity (fps)	2.75
			Max. Velocity (fps)	2.75
Discharge (cfs)	1.50		Normal Velocity (fps)	3.35
Diameter (inches)	10		Crit. Velocity (fps)	3.94
Ineffective Depth(ft)	0.00			
Length (feet)	909.0		freeboard @ outlet	1.58
Manning n	0.012		freeboard @ inlet	2.44
Entrance Vel. (fps)	0.00			
Entrance Loss (Ke)	0.50		Normal EGL (ft)	0.81
Slope	0.0046		Hyd.Jump d/s E	0.82



System: The Ranch at Swauk Creek

Reach: Burke Road Pipeline, MH #1 to MH #2 (Crosses Swauk Creek)

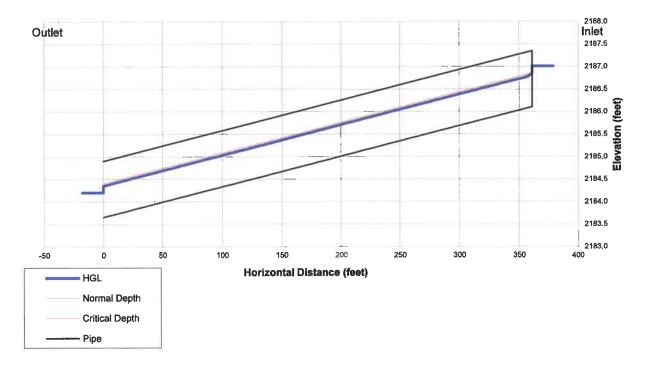
	<u>Outlet</u>	<u>Inlet</u>		
Identification	MH #2	MH #1	Normal Depth (ft)	0.45
Station	18+70	15+19	Critical Depth (ft)	0.55
Rim/Overflow Elev. (ft)	2181.75	2185.25	Froude No.	1.48
Invert Elevation (ft)	2178.90	2183.29	Avg. Velocity (fps)	5.01
Water Surf. Elev. (ft)	2179.31	2184.20	Min. Velocity (fps)	3.94
			Max. Velocity (fps)	5.03
Discharge (cfs)	1.50		Normal Velocity (fps)	5.03
Diameter (inches)	10		Crit. Velocity (fps)	3.94
Ineffective Depth( ft)	0.00			
Length (feet)	351.0		freeboard @ outlet	2.44
Manning n	0.012		freeboard @ inlet	1.05
Entrance Vel. (fps)	0.00			
Entrance Loss (Ke)	0.50		Normal EGL (ft)	0.84
Slope	0.0125		Hyd.Jump d/s E	0.82



System: The Ranch at Swauk Creek

Reach: Main Pipeline, Highway 97 Culvert to MH #1

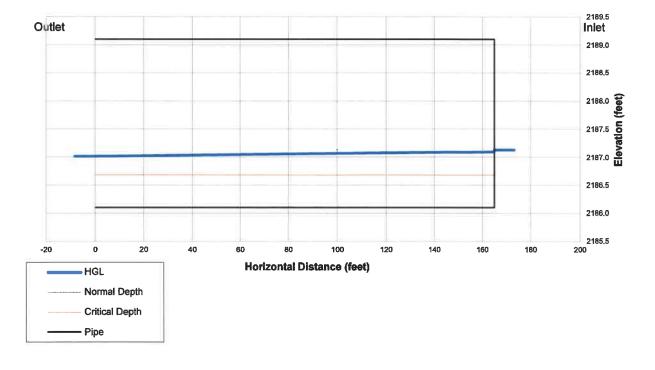
	<u>Outlet</u>	<u>Inlet</u>		
Identification	MH #1	D/S CULV	Normal Depth (ft)	0.70
Station	15+15	+15 11+54 Critical Depth (ft)		0.75
Rim/Overflow Elev. (ft)	2185.25	2189.10	Froude No.	1.15
Invert Elevation (ft)	2183.65	2186.10	Avg. Velocity (fps)	4.93
Water Surf. Elev. (ft)	2184.20	2187.01	Min. Velocity (fps)	4.52
			Max. Velocity (fps)	4.93
Discharge (cfs)	3.50		Normal Velocity (fps)	4.93
Diameter (inches)	15		Crit. Velocity (fps)	4.52
Ineffective Depth( ft)	0.00			
Length (feet)	361.0		freeboard @ outlet	1.05
Manning n	0.012		freeboard @ inlet	2.09
Entrance Vel. (fps)	4.52			
Entrance Loss (Ke)	0.50		Normal EGL (ft)	1.08
Slope	0.0068		Hyd.Jump d/s E	1.08



System: The Ranch at Swauk Creek

Reach: Main Pipeline, Existing Highway 97 Culvert

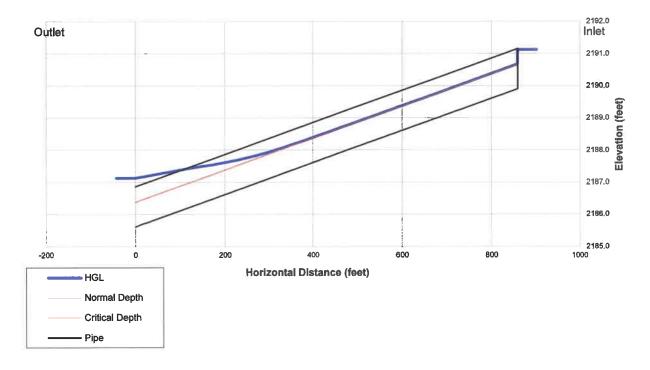
	<u>Outlet</u>	<u>Inlet</u>		
Identification	D/S CULV	U/S CULV	Normal Depth (ft)	3.00
Station	11+54	9+89	Critical Depth (ft)	0.58
Rim/Overflow Elev. (ft)	2189.10	2189.10	Froude No.	1.00
Invert Elevation (ft)	2186.10	2186.10	Avg. Velocity (fps)	1.81
Water Surf. Elev. (ft)	2187.01	2187.13	Min. Velocity (fps)	1.71
			Max. Velocity (fps)	1.92
Discharge (cfs)	3.50		Normal Velocity (fps)	0.50
Diameter (inches)	36		Crit. Velocity (fps)	3.62
Ineffective Depth(ft)	0.00			
Length (feet)	165.0		freeboard @ outlet	2.09
Manning n	0.012		freeboard @ inlet	1.97
Entrance Vel. (fps)	0.50		_	
Entrance Loss (Ke)	0.25		Normal EGL (ft)	3.00
Slope	0.0000		Hyd.Jump d/s E	3.00



System: The Ranch at Swauk Creek

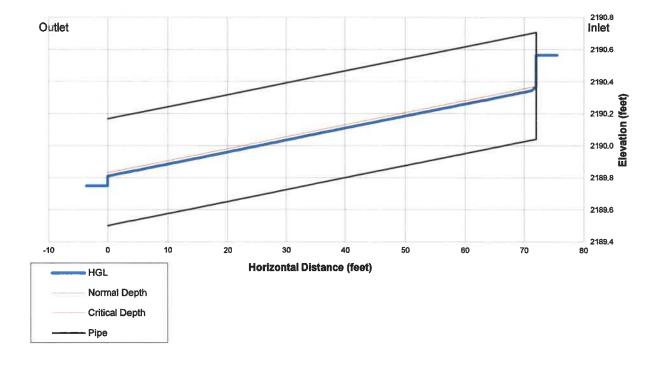
Reach: Main Pipeline, Inlet (D/S of Fish Screen) to Highway 97 Culvert

	<u>Outlet</u>	<u>Inlet</u>		
Identification	U/S CULV	INLET	Normal Depth (ft)	0.77
Station	9+89	1+30	Critical Depth (ft)	0.75
Rim/Overflow Elev. (ft)	2189.10	2192.40	Froude No.	0.95
Invert Elevation (ft)	2185.61	2189.90	Avg. Velocity (fps)	3.94
Water Surf. Elev. (ft)	2187.13	2191.12	Min. Velocity (fps)	2.85
			Max. Velocity (fps)	4.38
Discharge (cfs)	3.50		Normal Velocity (fps)	4.38
Diameter (inches)	15		Crit. Velocity (fps)	4.52
Ineffective Depth(ft)	0.00			
Length (feet)	859.0		freeboard @ outlet	1.97
Manning n	0.012		freeboard @ inlet	1.28
Entrance Vel. (fps)	0.00			
Entrance Loss (Ke)	0.50		Normal EGL (ft)	1.07
Slope	0.0050		Hyd.Jump d/s E	1.07



System: The Ranch at Swauk Creek
Reach: Fish Bypass Pipeline

	<u>Outlet</u>	<u>Inlet</u>		
Identification	CREEKF	SH SCRN	Normal Depth (ft)	0.31
Station	+72	+	Critical Depth (ft)	0.33
Rim/Overflow Elev. (ft)	2192.36	2192.40	Froude No.	1.14
Invert Elevation (ft)	2189.50	2190.04	Avg. Velocity (fps)	3.15
Water Surf. Elev. (ft)	2189.75	2190.57	Min. Velocity (fps)	2.89
			Max. Velocity (fps)	3.15
Discharge (cfs)	0.50		Normal Velocity (fps)	3.15
Diameter (inches)	8		Crit. Velocity (fps)	2.89
Ineffective Depth( ft)	0.00			
Length (feet)	72.0		freeboard @ outlet	2.61
Manning n	0.012		freeboard @ inlet	1.83
Entrance Vel. (fps)	0.00			
Entrance Loss (Ke)	0.50		Normal EGL (ft)	0.46
Slope	0.0075		Hyd.Jump d/s E	0.46



```
Hydraulic Analysis
```

System: The Ranch at Swauk Creek
Reach: Fish Screen Hydraulics

Design Event: Late Summer, Low Creek - 4 cfs Diversion (3.5 cfs to Ranch + 0.5 cfs Bypass)

#### BYPASS WEIR FLOW (Weir Gate or Stop Logs):

Weir Elev. (ft)
Weir Width (in)
H (ft)

TW WSEL (ft)

2191.38 Adjust so that HW WSEL~WSEL US of Screen
12 Adjust so that Discharge~Design Bypass Flow
0.29 Set at minimum required for fish passage
2190.57

TW WSEL (ft) 2190.57 HW WSEL (ft) 2191.67 Discharge (cfs) 0.5

#### DIVERSION WEIR FLOW (Over Stop Logs Through Paddle Wheel to Irrigation Pipe):

Weir Elev. (ft) 2190.17 Adjust so that Discharge~Design Flow to Irrigators

Weir Width (in) 12 Requested by Irrigators/USBR

H (ft) 1.25

TW WSEL (ft) 2191.12 WEIR IS BACKWATERED

HW WSEL (ft) 2191.42 Discharge (cfs) 3.5

#### **SCREEN:**

Bottom Elev. (ft) 2190.27 Adjust so that Submergence is >65% and <85%

Diam (ft) 2.0 Per Screen Shop

Top Elev. (ft) 2192.27

Min. WSEL (ft) 2191.57 65% Submergence
Max. WSEL (ft) 2191.97 85% Submergence

Screen Loss (ft) 0.25 Assumed

WSEL DS of Screen (ft) 2191.42 Channel IE @ Screen (ft) 2189.90

#### **AT FISH SCREEN:**

WSEL US of Screen (ft) 2191,67 Set so that WSEL at inlet of Diversion Channel~HEC-RAS Results

| Screen Submergence | 70% | Flow In (cfs) | 4.0 | Flow Out (cfs) | 4.0 |

#### **DIVERSION CHANNEL:**

Channel Length (ft) 30.00
Ave Bottom Widtch (ft) 2.00
Ave Sideslope (V ft/1 H ft) 1.50
Manning n: 0.03

IE at Screen (ft): 2,189.50
IE at Diversion (ft): 2,189.55
Depth at Screen (ft): 2.17
Flow Rate (cfs): 4.0
Depth, d (ft): 2.17
Flow Area, A (sf): 11.40
Wetted Perimeter, P (ft): 9.82

Hydraulic Radius, R (ft):

Velocity, V (fps):

Chanel Slope, S<sub>o (ft)</sub>:

Energy Slope, S<sub>f</sub> (ft/ft):

Velocity Head, V<sup>2</sup>/2g (ft):

Estimated Headloss:

1.16
0.00167
0.000167
0.00004
0.00019

Min. WSEL at Creek (feet): 2,191.67 This is what we need the roughened channel to produce at the creek to make this work.

# Appendix G Opinion of Probable Construction Cost

Bid Item	Description	Specificaiton	Quantity	Unit	Unit Cost	Cost
Division :	1 - General Requirements					
1	Mobilization/Demobilization (7.5%)	017113	1	LS	\$24,825	\$26,700
2	Traffic Control	015526	1	LS	\$5,000	\$5,000
3	Locate and Protect Existing Utilities	015615	1	LS	\$1,000	\$1,000
4	Temporary Erosion and Sediment Control	015713	1	LS	\$15,000	\$15,000
Subtotal	- General Requirements					\$48,000
Division :	2 - Existing Conditions				111	
5	Construction Surveying	022100	1	LS	\$12,000	\$12,000
6	Removal of Structures and Obstructions	024100	1	LS	\$3,500	\$3,500
7	Plug Pipe and Decomission Diversion at RM 7.71	024100	1	LS	\$2,500	\$2,500
Subtotal	- General Requirements	W	·			\$18,000
Division :	31 - Earthwork					
8	Clearing and Grubbing	311100	1.1	AC	\$5,000	\$5,500
9	Channel Excavation - River Mile (RM) 7.92	312300	1	LS	\$10,000	\$10,000
10	Channel Excavation - RM 7.71 (Option A Bid Item)	312300	1	LS	\$5,000	\$5,000
11	Excavation for Fish Screen Replacement	312300	1	LS	\$400	\$400
12	Structural Backfill for Fish Screen Replacement	312300	4.4	TN	\$35	\$154
13	Assistance with Fish Screen Installation	312300	1	LS	\$7,000	\$7,000
14	Installation of Transducer for Diversion Metering	312300	1	LS	\$3,000	\$3,000
15	Trench Excavation - Fish Bypass Pipeline	312300	1	LS	\$300	\$300
16	Pipe Bedding - Fish Bypass Pipeline	312300	11	CY	\$44	\$484
17	Select Backfill - Fish Bypass Pipeline	312300	7	CY	\$44	\$308
18	Final Backfill - Fish Bypass Pipeline	312300	1	LS	\$200	\$200
19	Trench Excavation - Irrigation Pipeline West of Highway 97	312300	1	LS	\$4,000	\$4,000
20	Pipe Bedding - Irrigation Pipeline West of Highway 97	312300	291	CY	\$44	\$12,804
21	Select Backfill - Irrigation Pipeline West of Highway 97	312300	188	CY	\$44	\$8,272
22	Final Backfill - Irrigation Pipeline West of Highway 97	312300	1	LS	\$4,200	\$4,200

# Kittitas County Conservation District The Ranch at Swauk Creek Diversion Improvement and Restoration Project Opinion of Probable Construction Cost - 90% Design

Bid Item	Description	Specificaiton	Quantity	Unit	Unit Cost	Cost
23	Controlled-Density Fill (CDF) Backfill - Irrigation Pipe West of Highway 97	312300	1.3	CY	\$250	\$325
24	Trench Excavation - Irrigation Pipeline East of Highway 97 (Option B Bid Item)	312300	1	LS	\$1,000	\$1,000
25	Pipe Bedding - Irrigation Pipeline East of Highway 97 (Option B Bid Item)	312300	227	CY	\$44	\$9,988
26	Select Backfill - Irrigation Pipeline East of Highway 97 (Option B Bid Item)	312300	154	CY	\$44	\$6,776
27	Final Backfill - Irrigation Pipeline East of Highway 97 (Option B Bid Item)	312300	1	LS	\$2,900	\$2,900
28	CDF Backfill - Irrigation Pipe East of Highway 97 (Option B Bid Item)	312300	1.3	CY	\$250	\$325
29	Diversion and Care of Water	312320	1	LS	\$24,850	\$24,850
30	Geomembrane Liner	313220	100	SY	\$15	\$1,500
31	Excavation Support and Protection	315000	1	LS	\$3,000	\$3,000
Subtotal	- Earthwork (Base Bid)	*				\$86,000
Subtotal	- Earthwork (Option A Bid Items)					\$5,000
Subtotal	- Earthwork (Option B Bid Items)					\$21,000
Subtotal	- Earthwork (Base Bid and All Optional Bid Items)					\$112,000
Division :	32 - Exterior Improvements					
32	Crushed Surfacing Base Course	321123	133	TN	\$35	\$4,655
33	Asphalt Paving	321216	5	TN	\$150	\$750
34	Imported Gravel-Cobble Mix - RM 7.92	325000	190	TN	\$75	\$14,250
35	Place Native Gravel-Cobble Mix - RM 7.92	325000	1	L\$	\$9,500	\$9,500
36	Place Imported Streambed Boulders - RM 7.92	325000	91	TN	\$125	\$11,375
37	Remove and Rework Native Streabed Boulders - RM 7.92	325000	1	LS	\$2,400	\$2,400
38	Place Native Gravel-Cobble Mix - RM 7.71 (Option A Bid Item)	325000	1	LS	\$2,900	\$2,900
39	Remove and Rework Native Streabed Boulders - RM 7.71 (Option A Bid Item)	325000	1	LS	\$4,000	\$4,000
40	Cottonwood Copse Planting (Option C Bid Item)	329000	3.5	AC	\$3,000	\$10,500
41	Streambank Revegetation - RM 7.92	329219	0.1	AC	\$10,000	\$1,000
42	Streambank Revegetation - RM 7.71 (Option A Bid Item)	329219	0.1	AC	\$10,000	\$1,000
43	43 Hydroseeding 329219 0.8 AC \$3,000 \$2					
Subtotal	- Exterior Improvements (Base Bid)			T = 3_0 1_77		\$46,000
Subtotal	- Exterior Improvements (Option A Bid Items)					\$8,000
	- Exterior Improvements (Option C Bid Items)					\$11,000
Subtotal	- Exterior Improvements (Base Bid and All Optional Bid Items)					\$65,000

# Kittitas County Conservation District The Ranch at Swauk Creek Diversion Improvement and Restoration Project Opinion of Probable Construction Cost - 90% Design

Bid Item	Description	Specificaiton	Quantity	Unit	Unit Cost	Cost
_	33 - Utilities					
44	15-inch Corrugated Polyehtylene (CPE) Irrigation Pipe - West of Highway 97	331115	364	LF	\$35	\$12,740
45	12-inch CPE Irrigation Pipe - West of Highway 97	331115	36	LF	\$25	\$900
46	10-inch CPE Irrigation Pipe - West of Highway 97	331115	340	LF	\$20	\$6,800
47	15-inch CPE Irrigaiton Pipe - East of Highway 97 (Option B Bid Item)	331115	877	LF	\$35	\$30,695
48	8-inch HDPE DR 32.5 Pipe for Fish Bypass	331117	72	LF	\$15	\$1,080
49	10-inch HDPE DR 32.5 Irrigation Pipe	331117	919	LF	\$22	\$20,218
50	Hang 10-inch HDPE Pipe on County Bridge	331117	1	LS	\$4,000	\$4,000
51	48-inch Pre-cast Concrete Manhole	331215	2	EΑ	\$3,500	\$7,000
52	Drain Valve Assembly	331217	2	EA	\$1,500	\$3,000
53	Canal Gate	331218	1	EA	\$1,500	\$1,500
Subtotal	- Utilities (Base Bid)			"		\$57,000
Subtotal	- Utilities (Option B Bid Items)					\$31,000
Subtotal	- Utilities (Base Bid and All Optional Bid Items)					\$88,000

TOTALS - BASE BID ITEMS		The plant Francisco
Construction Subtotal		\$255,000
Sales Tax	8.0%	\$20,400
Construction Subtotal		\$275,000
Construction Contingency	10.0%	\$27,500
Construction Subtotal		\$303,000

TOTALS - OPTION A BID ITEMS (CHANNEL RESTORATION AT RM 7.71)		
Construction Subtotal		\$13,000
Sales Tax	8.0%	\$1,040
Construction Subtotal		\$14,000
Construction Contingency	10.0%	\$1,400
Construction Subtotal	* * * * * * * * * * * * * * * * * * * *	\$15,000

9/17/2020

\$393,000

Bid Item Description	Specification	Quantity	Unit	Unit Cost	Cost
TOTALS - OPTION B BID ITEMS (IRRIGATION PIPELINE EAST OF HIGHW.	AY 97)		5.11		80.750
Construction Subtotal					\$52,000
Sales Tax		8.0%			\$4,160
Construction Subtotal					\$56,000
Construction Contingency		10.0%			\$5,600
Construction Subtotal					\$62,000
TOTALS - OPTION C BID ITEMS (COTTONWOOD COPSE PLANTING)			, n'hy		£44 000
Construction Subtotal			-		\$11,000
Sales Tax		8.0%			\$880
Construction Subtotal					\$12,000
Construction Contingency		10.0%			\$1,200
Construction Subtotal					\$13,000
TOTALS - BASE BID AND ALL OPTIONAL BID ITEMS		100010			ç illin isə bi
Construction Subtotal				T	\$331,000
Sales Tax		8.0%	Ì		\$26,480
Construction Subtotal			-		\$357,000
Construction Contingency		10.0%			\$35,700

**Construction Subtotal** 

<sup>1)</sup> Subtotals and totals are rounded to the nearest \$1,000.

<sup>2)</sup> Costs are in 2020 dollars. Actual construction costs may vary based on materials and labor costs at time of bidding.